# OPTIMIZATION OF WELL DESIGN AND LOCATION IN A REAL FIELD

### A REPORT SUBMITTED TO THE DEPARTMENT OF ENERGY RESOURCES ENGINEERING

### **OF STANFORD UNIVERSITY**

### IN PARTIAL FULFILLMENT OF THE REQUIREMENTS FOR THE DEGREE OF MASTER OF SCIENCE IN PETROLEUM ENGINEERING

By

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I certify that I have read this report and that in my opinion it is fully adequate, in scope and in quality, as partial fulfillment of the degree of Master of Science in Petroleum Engineering.

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## Abstract

As many fields around the world are reaching maturity, the need to develop new tools that allows reservoir engineers to optimize reservoir performance is becoming more demanding. One of the more challenging and influential problems along these lines is the well placement optimization problem. In this problem, there are many variables to consider: geological variables like reservoir architecture, permeability and porosity distribution, and fluid contacts; production variables such as well placement, well number, well type, and production rate; economic variables like fluid prices and drilling costs. All these variables, together with reservoir geological uncertainty, make the determination of a suitable development plan for a given field difficult.

The objective of this research was to employ an efficient optimization technique to a real field located in Saudi Arabia in order to determine the optimum well location and design in terms of well type, number of laterals, and well and lateral trajectories. Based on the success of Genetic Algorithm (GA) in problems of high complexity with high dimensionality and nonlinearity, they were used here as the main optimization engine. Both GA types, binary GA (bGA) and continuous GA (cGA), showed significant improvements over initial solutions but the work was carried out with the cGA because it appeared to be more robust for the problem in consideration.

After choosing the optimization technique to achieve our objective, considerable work was performed to study the sensitivity of the different algorithm parameters on converged solutions. When a definite conclusion could not be reached from this analysis, more tests were performed by combining cases and trying new directions to better discern the effects of the parameters. For example, dynamic mutation was implemented and it showed superior performance when compared to cases with fixed mutation probability. To further improve results given by the base optimization algorithm, it was hybridized with another optimization technique, namely the Hill Climber (HC). This step alone showed an improvement of about 12% over the base algorithm.

Once the different cGA parameters were determined, multiple optimization runs were performed to obtain a sound development plan for this field. More in-depth analysis was executed in an attempt to quantify the effect of some of the uncertain reservoir parameters in the model, some of the assumptions made during optimization, and some of the preconditioning steps taken before optimization. The studied effects included: uncertainty of aquifer strength, effect of using the accurate well index, and effect of using an upscaled model for optimization.

To fulfill aforementioned objectives, the location and design for a number of wells were optimized in an offshore carbonate reservoir in Saudi Arabia. The reservoir is mildly heterogeneous with low and high permeability areas scattered over the field. Applying the cGA to this reservoir showed that the optimum well configuration is a tri-lateral well. Studies regarding aquifer strength uncertainty and effect of using the accurate well index showed insignificant effect on optimized solutions. On the other hand comparing results from the fine and coarse reservoir models revealed that the best solutions are different between the two models. In general, solutions from different runs had different well designs due to the stochastic nature of the algorithm but there were some similarities in well locations.

# Acknowledgments

I would like to express my deepest gratitude to Professor Khalid Aziz, my research and academic adviser for his valuable contribution and insightful comments since the beginning of my work at Stanford. Completion of this work would not have been possible without his endless support and masterful guidance. I would also like to appreciate the input of Professor Louis Durlofsky and other faculty member of the Energy Resources Engineering Department at Stanford for their helpful remarks.

I would also like to acknowledge Mohammad Moravvej Farshi and Jerome Onwunalu for introducing me to the subject and helping to set up the scope of work. David Echeverria Ciaurri has also provided useful help regarding optimization procedures.

I am grateful for Saudi Aramco for financially supporting me and for providing the necessary model data to complete this study. My sincere thanks are also due to Reservoir Simulation Consortium (SUBRI-B) and Smart Fields Consortium, as being a part of these research groups has enlightened me with many ideas.

My special appreciation goes to my wife, Eman, and my parents. I am also indebted to all other friends and family members who supported me during this time. Most importantly, I would like to thank God for all the blessings and guidance he has given me.

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## Chapter 1

# **1. Introduction**

During the last two decades, horizontal wells have been used as the standard well type in oil field development projects. More recently, technological advancements have facilitated drilling of more complicated nonconventional well trajectories, which come in variety of forms such as Multilateral Wells (MLWs) and Maximum Reservoir Contact (MRC) wells. A distinctive example in this category is the well Shaybah-220 (Figure 1-1), which was completed in south eastern Saudi Arabia by the end of 2002. The well had 8 laterals and a total of 40,384 feet were drilled. Economic studies on the well showed a four-fold reduction in unit development cost and production testing indicated a five-fold increase in productivity index compared to horizontal wells completed in similar facies (Saleri et al., 2003). Several other studies have showed that the performance of nonconventional wells is superior in other areas as well compared to conventional wells. These advantages include extending reservoir contact length and drainage area, increasing net worth of the drilling investment, reducing operational drawdown pressure, and reducing producing gas-oil ratio (Horn et. al, 1997; Taylor et. al, 1997).

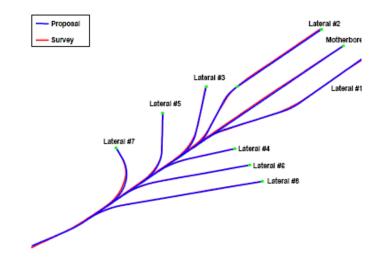


Figure 1-1: Shaybah-220 well plan and design (from Saleri et al., 2003).

However, the development of nonconventional wells poses several challenges. The real oil fields are complex environments due to heterogeneities, presence of geologic discontinuities (e.g. faults, fractures, and very high and low permeability zones), and geologic uncertainties. Moreover, given the fact that MLWs require more initial cost than conventional wells, the incremental value of the former might not be realized unless they are optimally placed within the reservoir. Engineering intuition is not sufficient to guarantee the optimum placement of these wells in most cases due to geological complexity and nonlinear nature of the problem. Similarly, the usual industry practice of trial and error to test multiple scenarios would rarely succeed to provide an optimum solution in the multidimensional well placement optimization problem. As a result, there is need for an optimization engine to evaluate the performance and viability of different well placement scenarios and determine their optimum design.

The main objective of this work is to employ an efficient optimization technique to identify a sound field development plan for a real field in Saudi Arabia. Optimized parameters include well type (producer or injector), well placement, well and lateral orientation, and number of laterals in each well. Further, we wish to investigate and improve the available optimization procedures. For this purpose, a review of the appropriate optimization procedures and an introduction of the problem are presented next.

#### **1.1. Literature Review**

Copious and diverse research works relating to well placement optimization have been discussed in the literature. While some studies focused on the placement problem, others have explored applying proxies to speed the optimization process. In addition, other studies tried to assess the performance of optimization under uncertainties. A survey of the most relevant studies is presented next.

To begin this survey, we would like to shed some light on some work that applied general optimization studies on well placement or design. Obi Isebor (2009) compared the performance of several gradient-free methods like the Genetic Algorithm (GA), direct search methods, and combinations of the two (GAs are explained in great detail in Chapter 2. A subset of direct search methods, the hill climber, is described in Section 4.1.2). He used these algorithms to optimize control variables with multiple nonlinear constraints on a channelized synthetic 2D model. He also applied penalty functions to account for constraint violations. He concluded that, for problems considered, General Pattern Search (GPS) with penalty functions perform the best followed by the combined GA and GPS algorithm.

Handels et al. (2007) and Wang et al. (2007) proposed different approaches for well placement optimization using gradient-based optimization techniques by representing the objective function in a functional form. They then calculated the gradient of this function and used a steepest ascent direction to guide the search. For the examples they considered, these methods seemed promising due to their efficiency in terms of number of simulation runs. The techniques were only applied to vertical wells and they expected more difficulty in applying them to problems with arbitrary well trajectories in complex model grids. Other issues they faced with these techniques include discontinuities in the objective function and convergence to local optima.

The next couple of paragraphs will give special attention to work done with GA, which is the optimization method used in this research. Bittencourt and Horne (1997) developed a hybrid binary Genetic Algorithm (bGA), where they combined GAs with the polytope method to benefit from the best features of each method. The polytope method searches for the optimum solution by constructing a simplex with a number of vertices equal to one more than the dimensionality of the search space. Each of the vertices is evaluated and the method guides the search by reflecting the worst point around the centroid of the remaining nodes. This work tried to optimize the placement of vertical or horizontal wells in a real faulted reservoir. The algorithm sought to optimize three parameters for each well: well location, well type (vertical or horizontal), and horizontal well orientation. The study also integrated economic analysis and some practical design considerations in the optimization algorithm.

Montes et al. (2001) optimized the placement of vertical wells using a GA without any hybridization. They tried to discern the effects of internal GA parameters, such as mutation probability, population size, initial seed, and the use of elitism. Their tests were applied on two synthetic rectangular models (a layercake model and a highly heterogeneous one). For the tested cases, they found that the ideal mutation rate should be variable with generation. Using random seeds for their problem showed little sensitivity while the use of elitism showed significant improvement. The population size study they performed suggested that an appropriate size was equal to the number of the variables in the problem. When they used very big populations, solution convergence was deterred as more poor quality chromosomes had to be evaluated. They also drew attention to issues like absolute convergence and stability of the optimization algorithm.

Emeric et al. (2009) implemented an optimization tool based on GA to optimize the number, location, and trajectory of a number of deviated producer and injector wells. They proposed a method to handled unfeasible solutions by creating a reference population consisting only of fully feasible solutions. Any unfeasible solution encountered in the optimization was repaired by applying crossover (refer to Section 2.3.1.1 for detailed description) between it and an individual from the reference population until a new feasible solution was obtained. They applied this technique in three full-field reservoir models based on real cases using two different strategies: the first one with the whole initial population defined randomly; and the second one by including an engineer's proposal in the initial population. Better results were observed in the second strategy and solutions were more intuitive for the tested case. They also suggested and tested an alternative optimization approach by only optimizing well type and number of an engineer's proposal. Although final results were not as good as the full

optimization, they concluded that this approach can be used when there is time limitation to perform the full optimization in complex cases.

Nogueira and Schiozer (2009) proposed a methodology to optimize the number and placement of wells in a field through two optimization stages. The procedure started by creating reservoir sub-regions equal to the maximum number of wells. Then, a search for the optimum location of a single well was performed in each sector. The second stage aimed to optimize well quantity through sequential exclusion of wells obtained from the first stage. After a new optimum number of wells is reached, the first stage is performed again until no improvement in the objective function is observed. This strategy showed efficiency when tested on a heterogeneous synthetic model with light oil. They optimized both vertical and horizontal wells in separate studies. They also concluded that the proposed modularization of the problem speeds up the optimization process for their problem of considertion.

Farshi (2008) converted a well placement and design optimization framework that was developed by Yeten et al. (2002) from bGa to a real-valued continuous Genetic Algorithm (cGA). A review of Yeten's work is surveyed later in this section. He found that the cGA provides better results when compared to the performance of bGA on the same synthetic models. Moreover, he implemented several improvements to the optimization process like imposing minimum distance between the wells and modeling curved wellbores.

Other studies sought to perform the task of well placement optimization under reservoir geological uncertainty. Guyaguler et al. (2000) applied a hybrid optimization algorithm, which also combines the features of bGAs with the polytope method. Furthermore, they utilized several helper functions including Kriging and Artificial Neural Networks (ANN) that act as proxies for the expensive reservoir simulations to reduce the optimization cost. The theory of the Kriging algorithm is based on the phenomenon that some variables that are spread out in space and time show a certain structure. The algorithm tries to understand this structure and move towards the direction that is expected to achieve

desirable results. ANNs are nonlinear statistical data modeling tools that are designed based on the aspects of biological neural networks. They seek to model complex relationships between inputs and outputs or to find patterns in data after completion of a training phase of the network that involves building a database from several simulation runs. This study optimized the locations of several vertical injectors for a waterflood project with the Net Present Value (NPV) as the objective function. Guyaguler et al. concluded that Kriging was a better proxy than neural networks for tested problems. They also conducted an uncertainty assessment study based on the decision theory framework. An extensive sensitivity study was performed as part of their study to determine the effect of the GA parameters.

Yeten et al. (2002) applied a bGA to optimize well type, location, and trajectory for nonconventional wells. Along with that, they developed an optimization tool based on a nonlinear conjugate gradient algorithm to optimize smart well controls. Several helper functions were also implemented including ANN, the Hill Climber (HC). In addition, they applied near wellbore upscaling, which approximately accounts for the effects of fine scale heterogeneity on the flow that occurs in the near-well region by calculating a skin factor for each well segment. The results of this study were presented on fluvial and layered synthetic models, as well as a section model of a Saudi Arabian field. An experimental design methodology was introduced to quantify the effects of uncertainty during optimization. The study also conducted sensitivity analysis in a similar manner to Guyaguler's (2002) study.

Rigot (2003) extended the optimization engine developed by Yeten et al. (2002) by implementing an iterative approach to improve the efficiency of multilateral well placement optimization. He divided the original problem into several single well optimizations to speed-up the optimization process and improves results. He also applied a proxy to avoid running numerical simulation if the expected productivity of a certain well was within the range of validity of the proxy.

Although previously commented studies provided promising optimization results, the used techniques consumed long optimization time. It is commonly unfeasible and computationally very expensive to conduct full optimization on some cases. To accelerate the optimization process, other work concentrated in designing proxies to the reservoir simulator. Pan and Horne (1998) used multivariate interpolation methods such as Least Squares and Kriging as proxies to reservoir simulation. The purpose of the first algorithm is to construct a function that has a simple known form to approximate some objective function. The behavior of this objective function is first observed through a number of simulations. Then, a function is constructed such that it minimizes the sum of the squared residual between data and the function values. To begin their study, they selected several well locations for numerical simulation as a sample to train the proxy. Then, Net Present Value (NPV) surface maps were generated using the two proxies. These maps were subsequently used to estimate objective function values at new points. They observed that the Kriging method provides more accurate means to estimate the objective function than the Least Squares interpolation in the tested examples.

Onwunalu (2006) applied a statistical proxy based on cluster analysis into the GA optimization process for nonconventional wells. His work also used Yeten's multilateral well model. The objective of applying the proxy is to reduce the excessive computational requirements when optimizing under geological uncertainty. The method is similar to the ANN method in terms of building a database of simulation results. The data base is then partitoned in clusters containing similar objects. The objective function of a new scenario can be approximated by assigning it to one of the constructed clusters. Additionally, his work extended the proxy to perform optimization of multiple nonconventional wells opened at different times. When simple wells were optimized the proxy provided a close match to the full optimization by simulation only 10% of the cases. This percentage increased to 50% when multiple nonconventional wells were optimized.

Although these studies showed the viability of using different optimization algorithms in field development problems, there is an apparent lack of real field applications. Some of

the algorithms were only tested on synthetic models and more testing is needed on real full-field reservoir models with complex geologic structures. This study approached the well placement and design optimization from this angle as we will elaborate in the next section.

#### **1.2. Problem Statement**

As stated earlier, while a MLW has high initial cost, its return on investment is usually higher than that of a conventional well. In this work, we try to optimize a field development scenario of a number of producers and injectors in terms of well configuration (number of laterals), and most importantly, the location of the mainbore and each of the laterals. Optimizing well locations also includes finding parameters that achieves the best performing well trajectory. These parameters include the length and orientation of each well segment. This results in a high number of variables, and thus, high problem complexity. A number of constraints are enforced to the potential wells to make sure they are physically achievable solutions. Some of these constraints are simple maximum and minimum bounds, while others are highly nonlinear and require careful handling.

Generally speaking, optimization problems search for the set of variables that achieves a maximum objective function according to the following equation:

Find 
$$x_{opt}$$
 such that:  $F(x_{opt}) \ge F(x)$  for all  $x \in \Omega$   
Subject to  $LB < C_n(x) < UB$  (1-1)

Here, x represents a vector containing problem parameters,  $\Omega$  symbolizes the search space domain, and C<sub>n</sub> corresponds to the problem constraints defined by upper and lower bounds. F stands for the objective function we are trying to optimize. For the well placement problem, this objective function can consider economic implications of the solution represented by the NPV of the project. However, since the field in question is operated by a national oil company (Saudi Aramco), the cumulative oil production is selected here as the objective function unless otherwise stated. OPEC countries are restricted by certain quotas and optimizing recovery is usually their ultimate goal rather than NPV.

As surveyed in the previous section, several optimization methods have been studied in the literature for similar problems. It must be emphasized that our method of choice should be capable of handling the complex nature of the problem, which in some cases involves more than 100 decision variables. Furthermore, the lack of analytical solutions in most cases and the nonlinearity and noncontinuity of oil field optimization problems limits the utilization of standard gradient based optimization methods (Montes et al., 2001). The complexity of the problem also implies that the objective function surface can contain several local optima, so the exploration criterion of the selected method must overcome converging towards such points. These reasons, along some others that are discussed in detail in Section 2.1, favor the employment of stochastic search methods that are typically successful in solving complex problems. GAs are one of the most common algorithms that belong to this category and they were chosen to solve this problem because they are easy to parallelize and hybridize. To our imperfect knowledge, the cGA in particular has only been tested on synthetic models for nonconventional well placement optimization and it is of interest to test its performance under real fields.

The objective of finding optimum well location and design was approached in this work through four main stages. Firstly, the performance of two variants of GA, the bGA and the cGA, was compared and a decision was made on the more robust algorithm for this problem. Secondly, the different internal algorithm parameters were tuned such that they consistently provide good results. This stage also included quantifying the contribution of adding helper tools and hybrid techniques to the search for optimum solutions. Thirdly, the tuned algorithm was applied to a full-field reservoir model based on a real case that we wish to optimize well locations and design for. The final stage involved investigating the reliability of the provided solutions by conducting uncertainty analysis and testing the effects of some of the assumptions made during optimization. The used code for optimizing multilateral well placement using the cGA was developed by Farshi (2008). Since the original code was designed for synthetic models, it has been modified to be compatible with any real field with complex geological setup and irregular grid sizes as detailed in later chapters. It is important, however, to note that the main contributions of the author are as indicated above. More enhancements were introduced to the code, including the implementation of a HC function, rejuvenation, and the minimum saturation screening. Results were generated for several examples that are presented in Chapter 4. Furthermore, the dynamic attributes of the code were modified to better suit the given field. In the descriptions that follow, the general approach and added improvements are discussed together.

The report will proceed as follows. In Chapter 2, a description of the optimization algorithm used in this study is detailed. Comparisons between bGA and cGA are made and parameter sensitivities are presented. Next, Chapter 3 provides a description of the reservoir model in question with the problem parameters and imposed constraints. It also focuses on practical implementation issues that arise when linking the optimization algorithm to the reservoir model. Then, Chapter 4 presents results obtained from the different cases run on the model. Additionally, an evaluation of the benefits of helper tools and of the uncertainties and assumptions in the optimization are discussed. Finally, Chapter 5 summarizes the conclusions of this work and gives suggestions for future work.

## **Chapter 2**

## 2. Main Optimization Engine

Before approaching the well optimization problem, a number of issues regarding the optimization engine need to be addressed. We have previously rationalized the appeal of applying GAs to such a problem. This chapter gives detailed description of the advantages and methodology of the algorithm. Then, it presents a comparison of the two GA types and a justification of choosing the cGA over the bGA through conducting a number of runs using each variant. Finally, the chapter discusses results of a sensitivity study on the internal search parameters of the algorithm. These parameters were exhaustively analyzed in order to reach a base case configuration to be used for well placement optimization problem in this field.

#### 2.1. General Description of Genetic Algorithms

The GA is a stochastic and heuristic search technique based on theory of natural evolution and selection. The basic idea revolves around survival of the fittest and solutions are evolved through mating (information exchange) of the best performing solutions. An occasional alternation of the fit solutions is allowed to occur to explore other parts of the search space or to avoid entrapment into local optima (Mitchell, 1996). Using GAs for the well placement optimization problem has been found to be ideal due to the following reasons:

- The algorithm can be easily parallelized because each of the individuals can be evaluated separately.
- The search for optimum is geared towards finding the global optimum rather than local optima.
- They perform well in problems where the fitness function is complex, discontinuous, noisy, changes over time, or has many local optima (Holland, 1992).

- The algorithm is capable of manipulating many parameters simultaneously.
- No gradients are required during the optimization process.
- Since the initial population is composed of multiple solutions rather than a single one, we have the opportunity to explore more of the search space at each generation.
- The algorithm can be enhanced and hybridized with other techniques.

### 2.2. Common GA Vocabulary

It should come as no surprise that most of the basic terminology used in GAs is inherited from Genetic Sciences. In the list below, the most common terms are explained (Yeten, 2003; Onwunalu, 2006).

- **Individual:** The set of parameters that defines a particular feasible solution within the search space.
- Chromosome: The coded notation of an individual.
- Gene: The coded representation of a single property within a chromosome.
- Generation: The iteration stage that the optimization process has reached.
- **Population:** The collection of individuals within the generation.
- **Fitness:** An evaluation of the quality of the objective function value for an individual. The fittest individual in a population would have the highest objective function value when compared to other individual in the same population.
- Seed: The initial population fed to the optimizer.
- Selection: A GA operator through which a number of the fittest individuals are kept in the next generation. This operator assures that every new generation is at least as good as the previous one.
- **Crossover:** Another operator that provides the main mating mechanism by which new chromosomes are created. The operator is designed such that an efficient information exchange and inheritance is achieved between generations.
- **Mating:** A mechanism used to ensure new genetic material is occasionally introduced to the chromosome. This operator also provides access to different areas of the search space.

- **Reproduction:** The process of applying GA operators described above to the current population or a portion of it in an attempt to evolve it into a better solution.
- Parents: Two fit individuals that are randomly selected to go through reproduction.
- **Offsprings:** Individuals that result after completion of the reproduction procedure.

#### 2.3. Binary vs. Continuous GAs

Two GA types are utilized in optimization problems, the bGA and the cGA. In bGAs, the optimization process embodies coding the value of each variable to its corresponding binary value, applying GA operators to the chromosome, obtaining the resulting offsprings and remapping them into the real space. On the contrary, cGAs use real-valued numbers directly. In addition to the GA advantages mentioned above, cGAs in particular are more appealing to use for this problem for the following reasons:

- The individual can assume any value in the search domain providing higher resolution when compared to the discrete bGA.
- It is easier to enforce variable adherence to the limits of the problem in cGA.
- The variable coding/decoding process in bGAs introduces translation deficiencies that can be prevented in cGA. A common problem is encountered when a desired transition between two adjacent values results in altering many binary bits in certain parameters. In other instances, the alteration of one bit can cause dramatic change in the value of other properties (Deb and Agrawal, 1995).

The chromosome in each variant of GA is formed by concatenating the properties of the solution. As an example, Equation (2-1) shows how the chromosome is represented in each GA for an arbitrary well, whose properties are listed in Table 2-1. The gene of each property has to accommodate the maximum value of that property, which explains the zeros to the left of some binary genes.

 $Binary = [0101101000000 \ 10111101101000 \ 011010101 \ 1101010010]$ Continuous = [2880, 12136, 213.3, 850] (2-1)

Property	Real Value	Maximum Var. Value	Required Binary Length	Binary Equivalent
x-coordinate	2880	15000	14	0101101000000
y-coordinate	12136	15000	14	10111101101000
Rotation angle	213.3	360	9	011010101
length	850	1000	10	1101010010

Table 2-1: Variable representation in binary and real space.

#### 2.3.1. Reproduction Operators

GA reproduction operators are designed to improve the performance of current individuals in the population. Three major operators are used in this algorithm, which are: selection, crossover, and mutation. The overall reproduction procedure is illustrated in Figure 2-1. In selection, the fittest member of each generation is carried to the next one (also called elitist selection). Moreover, members of the current population are selected as potential parents for individuals in the next generation according to a user-defined cut-off value. A fitness-proportionate selection is applied for this study; in which fitter individuals are more likely, but not certain, to be selected. The following rank weighting formula was used to calculate the probability of selecting an individual as defined by Farshi (2008):

$$p_{n} = \frac{\left(N_{select} + 1 - n\right)^{r}}{\sum_{i=1}^{N_{select}} (i)^{r}},$$
(2-2)

where  $N_{select}$  is the lowest rank of an individual that can be selected as a potential parent, n is the ranking of the current individual, and r is a ranking scale factor ( $\geq 1$ ) that is applied to give higher weight to fitter individuals. Individuals that have a rank lower than  $N_{select}$  will be discarded and not selected for further reproduction. The other two GA operators are explained in more detail in the following sections.

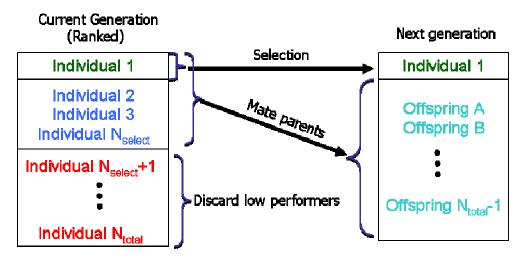


Figure 2-1: Reproduction procedure in GAs.

#### 2.3.1.1. Crossover

The crossover operator is intended to simulate the analogous recombination process that occurs in genetic chromosomes during reproduction. Crossover has been described as the key element that distinguishes GAs from other optimization methods. This is because it achieves an efficient transfer of information between successful candidates. With crossover, individuals have the opportunity to evolve by combining the strengths of both parents. On the other hand, an individual does not communicate with others in the population when there is no crossover. In other words, each individual is exploring the search space in its immediate vicinity without reference to what other individuals might have discovered (Koza et al., 1999).

In bGAs, the simplest form of crossover can be implemented by cutting the parents' chromosomes at a random point and swapping the two resulting portions (Figure 2-2), which is called single-point crossover. Other common forms of crossover include multipoint crossover, in which several points of exchange are set; and uniform crossover, where the offspring's genome value can be taken from either parent with a 50/50 probability. Crossover is only performed on a certain percentage of the population according to the crossover probability,  $P_{xo}$ .

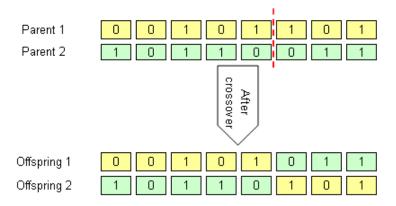


Figure 2-2: Simple crossover in bGAs.

Using the aforementioned swapping technique in cGAs means that the properties of the current generation would be carried on to the next generation without introducing any new values, which does not achieve the desired diversity in the generation. Losing diversity in the population makes it more uniform, consequently leading to premature convergence to a suboptimal solution. This problem, however, can be reduced by utilizing crossover with blending as defined by Radcliff (1991) using the following equation:

$$P_{i}^{new} = \beta \cdot P_{Mi} + (1 - \beta)P_{Fi}, \ 0 \le \beta \le 1,$$
(2-3)

where  $P_i^{new}$  is the i<sup>th</sup> variable in a new individual, and  $P_{Mi}$  and  $P_{Fi}$  are the property values of the same variable from the mother and father individuals, respectively.  $\beta$  is a blending coefficient that can remain constant for each crossover operation, or can be randomly chosen for each single property. In this study, we opted for the latter approach because it is more likely to diversify the population (Farshi, 2008). The limits of  $\beta$  bounds values of the new property between that of the mother ( $\beta = 1$ ) and that of the father ( $\beta = 0$ ). Again, the number of variables within an individual that will undergo the above process is determined by  $P_{xo}$ .

#### 2.3.1.2. Mutation

In contrast to crossover, which is responsible for the exploitation and evolution part of the evolution process; mutation adds a randomness factor to the search process to allow the solution to explore new areas of the search space. The main concept of mutation is to cause small random alterations at single points in the chromosome. The number of

mutation occurrences is governed by the mutation probability,  $P_{mut}$ , which is usually small (in the order of 0.01 to 0.1). Since any bit of a binary chromosome can only take two values, mutation can be applied in bGAs by switching the value of bits that are selected for mutation as shown in Figure 2-3.

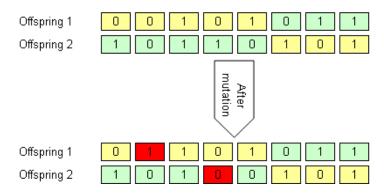


Figure 2-3: Mutation in bGAs.

Although the implementation in cGAs is different, the main function of mutation remains the same. Mutation in this algorithm can be attained by adding a normally distributed random number to the variable selected for mutation as shown in Equation (2-4) (Haupt and Haupt, 2004):

$$P_i^{new} = P_i^{old} + \sigma \cdot N(0,1), \qquad (2-4)$$

where  $P^{old}$  and  $P^{new}$  are the property values before and after mutation, respectively. N is a randomly distributed number between zero and one, and  $\sigma$  is the standard deviation of this property in the current population. The added value is scaled by the standard deviation of the current property to make sure the property does not exceed its feasible range.

#### 2.3.1.3. Overall Optimization Workflow

The reproduction procedure described above is just one part of the optimization loop. Figure 2-4 shows a flow chart of the complete procedure. In a step-wise fashion, the main GA optimization stages are:

1. Define optimization parameters and their limits.

- 2. Create a diverse initial population that honors the limits defined above. These potential solutions can be selected randomly or intuitively based on experience.
- Evaluate the fitness of each individual by obtaining its objective function, which is calculated from reservoir simulation output. All simulations in this study were performed using Schlumberger GeoQuest's commercial reservoir simulator, ECLIPSE 2007a.
- 4. Rank the current population according to the value of the objective function.
- 5. If the predefined convergence criterion is met, exit and analyze the results. If not, proceed to step 6. Convergence can be declared when one or all of the following conditions are met:
  - a. All individuals in the current population become very similar.
  - b. There is no improvement in the objective function for a number of consecutive generations.
  - c. A maximum generation number is reached (applied for this study).
- 6. Apply reproduction operators described in the previous section to the current population.
- 7. Go back to step 3.

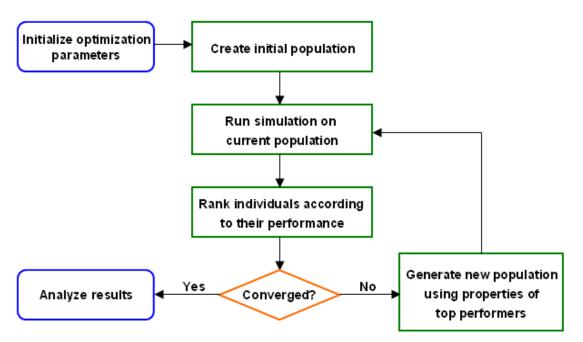


Figure 2-4: Flowchart of the overall optimization procedure using GAs.

#### 2.3.2. Performance Comparison

After understanding the mechanism of the two variants of GA, it is of interest to test which of them is more suitable for this problem by comparing their performance. The following exercise was designed to achieve this objective by finding the best location and configuration for three deviated producers and two deviated injectors completed in the reservoir described in Section 3.1. A population size of 30 was used, which is equal to the number of variables. The optimization ran for 35 generations, which seems more than sufficient for the size of this problem. A rationale of the choice of these numbers is discussed in Sections 2.4.2 and 2.4.3. This results in 1050 simulations. Cumulative oil production over a ten-year period is used as an objective function. All other GA and optimization parameters were kept the same for the two GAs.

Binary coding of problem variables resulted in a chromosome length of 270 bits. To provide more efficient crossover for this chromosome, the implemented bGA involves using multi-point crossover with a total crossover points equal to the number of well segments. Mutation had to be controlled for this exercise in order to make it only possible for bits that do not produce invalid solutions. For instance, the chromosome of a wellbore that has a z-coordinate of 4550 feet is represented in binary bits by 1000111000110. If the limits in this coordinate were between 4470 and 4620 feet, mutating any of the first six bits would generate invalid solutions. This kind of check was performed for all variables.

Both algorithms were run six times with a different random initial population for each run. Figure 2-5 compares the evolution of the objective function for the best individual in three of the runs for each method, as well as the averages of the six runs. A number of observations can be made from this plot. First, the cGA evolves the solution in a gradual fashion. Conversely, the bGA in general shows some jumps followed by flat regions. Second, the average of the two methods is close until the end of the run, where cGA shows slight advantage. Third, the individual runs in the cGA are more clustered around

its average than the bGA. This might give an indication about the robustness of the algorithm; we are more likely to get a good answer with cGA if fewer runs are performed.

Another measure of robustness is provided by the repeatability of the algorithm. The moving average for each algorithm was calculated by averaging objective function results by the end of optimization after an additional run has been performed. As previously mentioned, each algorithm was run six times. This means that the moving average by the end of the third run, for example, is the mean of the objective function of the best individual from these three runs when the run has ended. This average for cGA and bGA is plotted in Figure 2-6 along with the percentage change in the average after an additional run is added. The plot indicates that the average in cGA is stabilized after around three runs. We consider the average to be stabilized if the change from adding an additional run was within  $\pm 1\%$  because it is unlikely that a decision would be changed based on such a small change. In contrast, the bGA required five runs for its average to obtain a more representative average.

Another advantage that gives more preference for the cGA is the lenience it provides in handling the set of constraints and variables for the problem of interest. Some constraints (particularly vertical well limits as we will see in Section 3.3.2) are difficult to capture with the bGA. Since invalid reproduced solutions are handled by repeating the whole reproduction procedure, the reproduction step in bGA consumes considerably more time. On average, reproduction was completed in about 42 seconds per generation in bGA as opposed to just 3 seconds in cGA, which increases the computational cost of optimization. Other optimization steps were completed in around the same time for both algorithms.

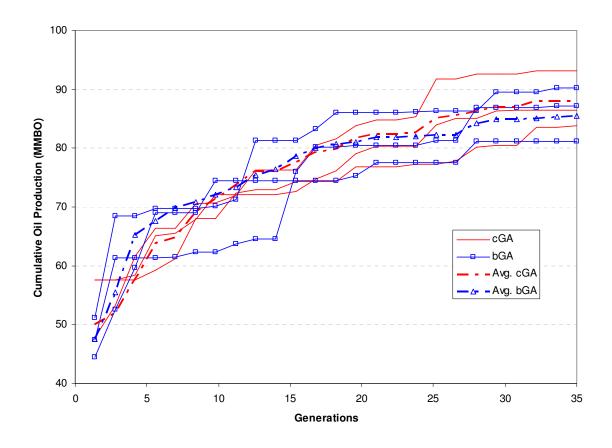


Figure 2-5: Fittest individual performance comparison of three different runs and the average of the total six runs from the bGA and the cGA.

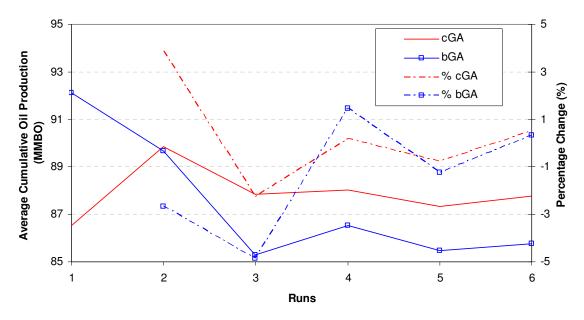


Figure 2-6: Moving average and percentage change of the objective function of the fittest individual as more runs are added in the bGA and cGA.

#### 2.4. Sensitivity to cGA parameters

Due to the stochastic nature of GAs, the final solution of the same problem is usually different when the algorithm is run a number of times. This is due to the different GA probabilities, selection fractions, initial population, and number of generations. In this section, the effects of each of these factors on the final solution given by the GA were studied. A better understanding of the effect of each parameter might help us in empowering the search process of the algorithm. Moreover, setting all parameters to their best tested value would provide us with a starting ground to apply the algorithm on the well placement optimization for this field.

#### 2.4.1. Sensitivity to Operators' Probabilities and Fractions

This test was performed to tune the effect of each GA operator. Several studies have indicated that crossover and mutation probabilities have the most effect on the results (Guyaguler, 2002; Yeten, 2003; Farshi, 2008). The selection fraction  $(f_{select} = N_{select}/N_{total})$  is also included in this study to account for the third GA operator, selection.

The test was designed by selecting a low, a medium, and a high value for crossover and mutation probabilities; and two values for the selection fraction. These values and all other GA parameters used for this run are listed in Table 2-2. We ran the optimization by varying one parameter at a time while fixing all other parameters. Note that the population size and maximum generation value remain constant for this study. Separate investigations for these two parameters are presented in the following two sections. Each case is repeated three times to reduce the stochastic effect of the algorithm. Also, the same initial population was used to eliminate the effect of initial population. This results in 54 different runs. The objective function is the same to what was defined in the previous example. The quality of each run was determined by averaging the objective function value of the fittest individual from the three runs, which are listed in Table 2-3.

<b>GA Parameter</b>	Value
Population size	20
Maximum generation	30
Crossover probability	[0.4, 0.6, 0.8]
Mutation probability	[0.01, 0.05, 0.1]
Selection fraction	[0.5, 0.8]
Ranking scale	2

Table 2-2: GA parameters used in the sensitivity analysis.

Table 2-3: Average fitness for the different GA parameters used.

	$f_{select} = 0.8$		$f_{select} = 0.5$			
P <sub>xo</sub> P <sub>mut</sub>	0.4	0.6	0.8	0.4	0.6	0.8
0.01	53.9	54.2	53.1	50.7	53.8	56.1
0.05	52.6	56.6	66.1	54.3	59	63.2
0.1	49.2	56	56.2	51.5	57.9	61.6

In general, higher crossover probability and medium mutation probability achieved better results. This is consistent with the conclusions of Yeten (2003) and Farshi (2008), where the optimum  $P_{xo}$  values were found to be between 0.8 and 1.0 and optimum  $P_{mut}$  values were in the neighborhood of 0.04 to 0.05. No firm conclusion could be drawn about the effect of the selection fraction by looking at the average results. However, selecting half of the population as potential parents seems to be more consistent.

An interesting phenomenon was observed in the solution evolution of different  $P_{mut}$  values plotted in Figure 2-7. While the performance of high  $P_{mut}$  (shown in green) is clearly lower than the other two probability values, low  $P_{mut}$  (blue) appears to be better in the early stages of the optimization than the medium value (red). This advantage is reduced as we reach the later parts of optimization and low  $P_{mut}$  seems to cause premature convergence as no improvement is observed in the last 15 generations. A similar study by Montes et al. (2001) and Emerick et al. (2009) reached the same conclusion. They

suggested the need for low mutation rates in the beginning because allowing high rates at this stage would overshadow the role of crossover. In later generations, however, a high mutation rate is needed as solutions become more evolved and homogeneous. This high mutation rate maintains diversity in the population, which increases the possibility of finding optimum solutions. Results in Figure 2-7 are for  $P_{xo} = 0.8$  and a selection fraction of 0.5 but most other combinations showed similar trends.

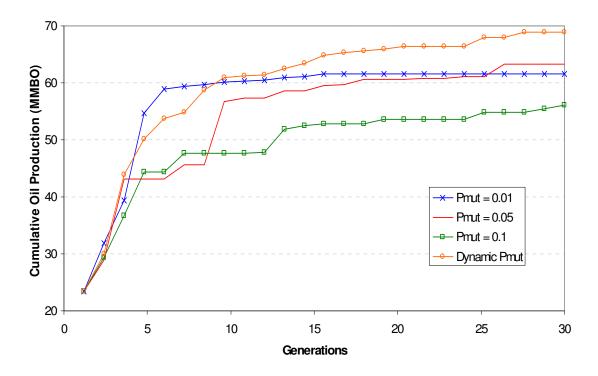


Figure 2-7: Fittest individual performance comparison averaged over three runs for different mutation probabilities.

To exhibit the advantages of medium and low mutation probabilities, an additional run was made with a dynamic mutation probability. The orange curve shows the result for this run where  $P_{mut}$  was set to 0.01 until the end of the tenth generation, then increased to 0.05 thereafter. This change shows an improvement of approximately 8% over  $P_{mut} = 0.05$ . To confirm the above results, the same procedure was repeated with a different initial population, results of which are plotted in Figure 2-8. The benefits of implementing dynamic mutation are even more apparent in this example. Nonetheless, the point at which the low mutation probability stops evolving the solution is different here (after around 14 generations compared to 10 in the previous example). This makes it

interesting to change the mutation probability automatically when the low value stops improving the solution after a consecutive number of generations instead of using a fixed generation as implemented here. This improvement, however, was not implemented due to time limitations.

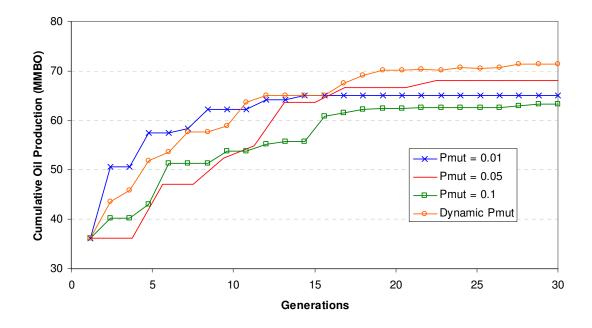


Figure 2-8: Fittest individual performance comparison averaged over three runs for different mutation probabilities when a different initial population was used.

#### 2.4.2. Sensitivity to Initial Population

As previously discussed, GAs are seed dependent algorithms. Fitter initial populations are more likely to produce better solutions. The population size depends on the nature, complexity, and number of variables of the problem. Typically, the population is generated randomly such that it covers the entire range of possible solutions. A couple of studies have suggested that problems of moderate complexity problems should have a population size equal to the chromosome's bitstring length in bGA (Goldberg, 1989; Alander, 1992; Montes, 2001). An analogous population size for cGAs has not been established in the literature; hence, a simple test was designed to investigate the issue.

Traditionally, the rule of thumb is to make the population size equal the number of variables in the problem, which we based the Base Case design on. Two more cases were

run. Case 1 had an initial population size that is double the number of variables. All individuals in this initial population are evaluated but the optimization proceeded with only the better half. Case 2 had the same initial population as in Case 1 but the population is reduced dynamically as the optimization progresses. The population size of each case is schematically explained in Figure 2-9. The run and well specifications are similar to those defined in the previous section with  $P_{mut} = 0.01$  changing to 0.05 after the tenth generation,  $P_{xo} = 0.8$ , and  $f_{select} = 0.5$ .

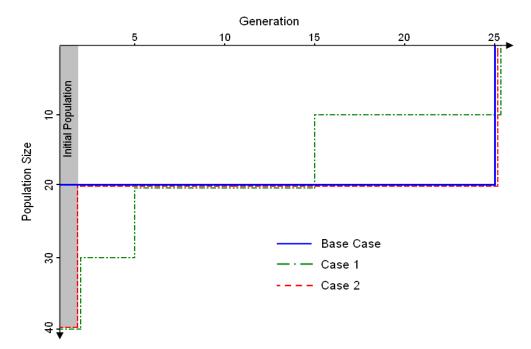


Figure 2-9: Population size for each generation in the three cases. The size is being held constant for the Base Case and dynamically assigned for Cases 1 and 2.

Each case was repeated three times and average results of the fittest individual are plotted in Figure 2-10. Case 1 showed improvement over the Base Case only at the beginning of optimization. The reasoning behind this occurrence becomes clearer after looking at the objective function of the top five individuals from each case listed in Table 2-4. Because of the larger initial population for Case 1, fitter individuals were introduced, which translated to better solutions in the beginning of the run. However, the algorithm in the Base Case was eventually able to evolve and reach similar objective function values to those returned by Case 1 by the end of the run. Case 2, on the other hand, performs better from the beginning and maintains the advantage until the end of the run. The difference between the Base Case and Case 2 amounted to around 6% by the end of the run. This result was also achieved with fewer simulations (460 simulations as opposed to 520 simulations). Note that each tested case had 18 optimization variables. It might be difficult to generalize these conclusions on more complicated scenarios.

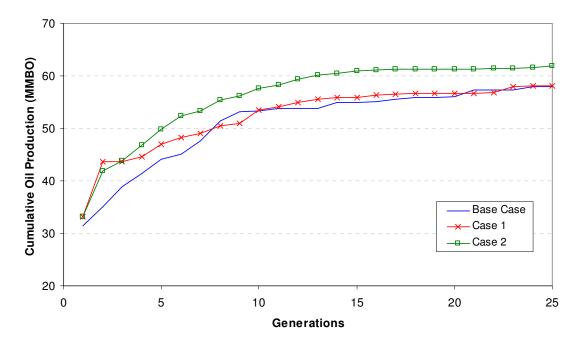


Figure 2-10: Fittest individual performance comparison averaged over three runs after using a constant population size for the Base Case and two designs for a dynamic population size in Cases 1 and 2.

Table 2-4: Comparing the fitness of top five individuals when a bigger initial population
is used

Individual	Cumulative Production (MMBOD)		
muiviuuai	Case 1	Base Case	
1	38.9	31.4	
2	29.9	26.7	
3	28.7	24.2	
4	22.6	21.5	
5	22.5	19.9	

#### 2.4.3. Required Number of Generations

An important question that we must answer before applying this algorithm to a real field is how long the optimization should run. Without consideration to urgencies that might come up in a real scenario, the interest here is to find out how many generations are required for a certain optimization to converge. This, of course, is also dependent on the complexity of the problem represented by the number of variables. To discern the effect of number of variables on the maximum required generation, three cases were optimized for 60 generations. The three cases were picked to represent a relatively simple, a moderately complicated, and a complex problem. The first case contains three deviated producers and two deviated injectors. The second and third cases consist of the same number of wells but each well has two and four laterals, respectively. The resulting number of variables (from Equation 3-3 to be discussed in Chapter 3) for this set-up is 30, 70, and 110 for the three cases. Each case was repeated three times and the average results of the fittest individual are plotted in Figure 2-11. Note that the objective from this exercise is not to compare the performance of the three cases but rather to select an appropriate maximum number of generations for each case. Assuming that convergence have occurred when no improvement in the objective function has taken place for ten consecutive generations, it appears that 25 generations are sufficient to provide a converged solution when 30 variables are used for the analyzed case. This number increased to around 32 when the number of variables was increased to 70. When 110 variables were used, 45 generations were required to reach a converged solution.

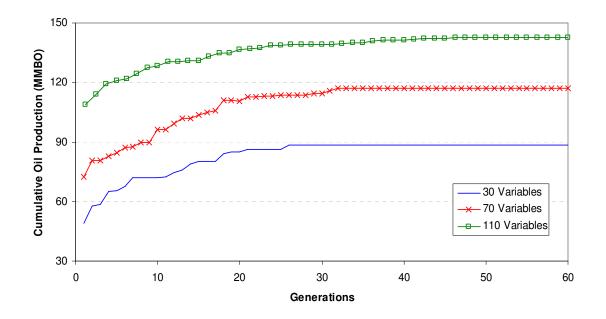


Figure 2-11: Convergence of the fittest individual averaged over three runs for problems with different number of variables.

## 2.5. Concluding Remarks

In this chapter, we have justified the suitability of using GAs in high dimensional optimization problems such as well placement and design optimization. We have further shown that the cGA yields better results than the bGA for this particular field, and therefore, it was used as the main optimization algorithm. Sensitivity analysis was performed to determine the best combination of internal cGA parameters. This analysis showed that dynamic mutation, 0.8 crossover probability, and 0.5 selection fraction returned the best results. A dynamic population size also showed an improvement in results with less number of simulations. For the tested case, it was found that running the optimization for three times attained a representative average of the objective function. Finally, the number of needed generations depends on the complexity of the problem. 25, 32, and 45 generations were needed to get a converged solution when 30, 70, and 110 variables were used, respectively.

Having decided on an optimization algorithm to be used for this problem, the next chapter will describe the needed steps to smoothly apply this algorithm to the reservoir model at hand.

# Chapter 3

# 3. Practical Framework of Well Placement Optimization

Within the optimization process, numerous interactions take place between the GA and the reservoir simulator. The two parts have to be completely compatible in order to have a trouble-free process and reliable solutions. The purpose of this chapter is to establish a good understanding of the reservoir model and the optimized parameters. Such an understanding will ease integration between the two parts. This chapter also describes how to ensure that invalid solutions are prevented by adhering to the problem's constraints. Implementation of some of the important nonlinear constraints is demonstrated along with the resulting optimization improvements from this step. Lastly, some of the important interaction steps between the optimizer and the reservoir model, such as the information exchange mechanism and objective function calculation, are briefly explained.

### 3.1. Reservoir Model Description

The model is for a carbonate reservoir in offshore Saudi Arabia. In all subsequent text, this reservoir will be referred to as the S1 reservoir. The reservoir extends over a 26 by 41 km area and is currently under evaluation for full development. As can be seen in Figure 3-1, oil has accumulated due to a dome stratigraphic trap. Although only 14 vertical observation wells have been completed in S1, many wells were drilled to a deeper reservoir in the same field. Therefore, many core samples and open hole log data are available for S1 reservoir. From these data, it has been recognized that permeability is mildly heterogeneous (Figure 3-1). While most areas have a permeability of around 200 mD, high permeability (1-2 Darcy) areas are scattered around the field. An areally isotropic permeability is used in the model with a vertical to horizontal permeability ratio

of 0.05. Other important reservoir, rock, and fluid properties are listed in Table 3-1 and 3-2. Because the field is operated above the bubble point pressure, the simulation model only contains the oil and water phases.

Table 3-1: S1 reservoir properties		
OOIP	2.4 BSTB	
$\Phi^*$	23%	
k*	300 md	
k <sub>z</sub> / k <sub>h</sub>	0.05	
Average gross thickness	151'	
T*	145 °F	
P* <sub>res</sub>	1738 psig	
c <sub>r</sub> *	$4.5 \times 10^{-6} \text{ psi}^{-1}$	

Table 3-1: S1 reservoir properties

\* for average

Table 3-2: Fluid properties

P <sub>buble</sub>	876 psia
Solution GOR	224 scf / STB
Crude Grade	28.9 API
μ <sub>o</sub>	4.8 cp
Bo	1.13 BBL / STB
C <sub>o</sub>	6.5x10 <sup>-6</sup> psi <sup>-1</sup>
$\lambda_{ m w}$	1.16
$\mu_{\rm w}$	0.52 cp
B <sub>w</sub>	1.00 BBL / STB
$c_{ m w}$	3.00x10 <sup>-6</sup> psi <sup>-1</sup>

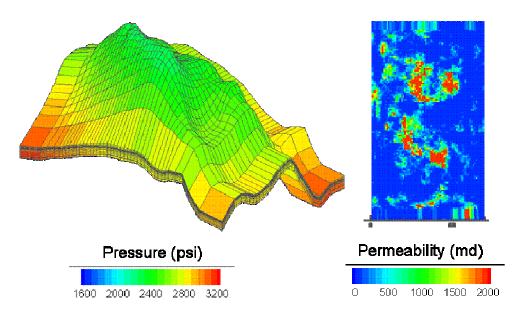


Figure 3-1: Average reservoir pressure and permeability maps for S1 reservoir.

The reservoir model constructed by Saudi Aramco is  $69 \ge 122 \ge 14$  (117,852 total cells). A structured grid is used and cell dimensions vary in each direction, which contributes to the geometrical complexity. Since the optimization process involves thousands of simulations, an upscaled version of the model was obtained. The fine model was coarsened with a ratio of 3:1 in each of the two areal directions while keeping the vertical resolution to contain the thin shale layers existing in the reservoir. The resulting coarse model dimensions are 23 x 41 x 14 (13,202 total cells). Simulations on the upscaled model were faster than those on the fine model by approximately a factor of 40. Hence, this model was used to obtain all results to be presented in Chapter 4, unless otherwise specified. In Section 4.5, a final optimization run on the fine model is discussed and the results are compared with the coarse model.

#### 3.2. Problem Variables

The optimized variables in this problem were chosen such that they possess three important characteristics. Firstly, they have to be independent because each variable is selected and mated randomly with other individuals. Choosing independent variables also allows us to work with the lowest possible set of variables for the problem. Reducing the number of variables would help to reduce the complexity of the problem and ease the optimization process. Secondly, the variables should have significant physical meaning such that there is a strong connection between them and the objective function values. By doing so, GA operators are more capable of directing the search towards the optimum solution during the information exchange process. Finally, the variables should be easy to handle during the constraint enforcement stage. More elaboration on this issue will follow in the next section.

In this work, we use the variable set defined by Farshi (2008). Since the well's mainbore can be represented by a straight line in the 3D space, six variables are sufficient to define its trajectory. These variables are: the three coordinates of the midpoint ( $x_{mid}$ ,  $y_{mid}$ ,  $z_{mid}$ ), total well length ( $L_{tot}$ ), vertical well distance between the tow and the heel ( $Z_h$ ), and the top-view rotation angle ( $\Theta$ ). Using  $Z_h$  as a variable is very handy in creating wells within the vertical limits of the reservoir. When it comes to laterals, four variables would completely define their orientation since one degree of freedom is lost as they are fixed to the mainbore. As a consequence, defining one variable (junction position relative to the total mainbore length,  $J_p$ ) can replace the three midpoint coordinates. The other two lengths and angle variables complete the lateral's definition. Figure 3-2 provides a visualization of the variable set. Other dependent parameters that are needed during optimization, such as heel and toe coordinates of the mainbore and laterals, can be calculated from the independent variables stated above according to the following equations:

$$\begin{aligned} x_{heel,toe}^{well} &= x_{mid}^{well} \pm \frac{1}{2} L_{xy}^{well} \sin \theta^{well} & x_{heel}^{lat} = x_{heel}^{well} + J_p \left( x_{toe}^{well} - x_{heel}^{well} \right) \\ y_{heel,toe}^{well} &= y_{mid}^{well} \pm \frac{1}{2} L_{xy}^{well} \cos \theta^{well} & z_{heel}^{lat} = z_{heel}^{well} + J_p \left( y_{toe}^{well} - y_{heel}^{well} \right) \\ z_{heel,toe}^{well} &= z_{mid}^{well} \pm \frac{1}{2} Z_h^{well} & L_{xy} = \sqrt{L_{tot}^2 - Z_h^2} \end{aligned}$$
(3-1)

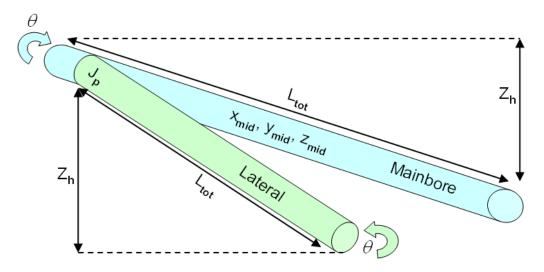


Figure 3-2: Well parameter representation in the well optimization problem.

With the optimization variables in place, a chromosome can be constructed by concatenating the producers' properties until the total number of producers is reached  $(P_{num})$ , followed by the injectors' properties until we reach total number of injectors  $(I_{num})$ . The chromosome is eventually represented as a vector containing all parameters to be optimized as shown in following equation:

$$Chromosome = \{..., prod(n), ..., prod(P_{num}), ..., inj(m), ..., inj(I_{num})\}$$

$$prod(n) = [(x_{mid}^{mb}, y_{mid}^{mb}, z_{mid}^{mb}, L_{tot}^{mb}, Z_h^{mb}, \theta^{mb}), ..., (J_p^{lat(i)}, L_{tot}^{lat(i)}, Z_h^{lat(i)}, \theta^{lat(i)}), ....]$$

$$inj(m) = [(x_{mid}^{mb}, y_{mid}^{mb}, z_{mid}^{mb}, L_{tot}^{mb}, Z_h^{mb}, \theta^{mb}), ..., (J_p^{lat(j)}, L_{tot}^{lat(j)}, Z_h^{lat(j)}, \theta^{lat(j)}), ....]$$
(3-2)

As we are basing the population size on the number of variables, it is very important to use a low number of variables at any optimization. This number is proportional to the number of wells and laterals in each well as demonstrated by Equation (3-3). Increasing the number of wells and laterals can substantially increase optimization time and complexity.

$$Var_{count} = Well_{count} (6 + 4(Lat_{count})),$$
(3-3)

 $Var_{count}$  above is the total number of decision variables in the problem,  $Well_{count}$  is the total number of wells, and  $Lat_{count}$  is the number of laterals in each well. A description of the procedure of creating new individuals using this set of variables is presented next.

#### **3.3.** Constructing the Initial Population

Creating an individual that contains a number of wells with the desired variables is not a trivial task. As the model being used for optimization is for a real field, we had to make sure all proposed solutions are feasible. This means that they must be within the physical constraints for that particular field. Several constraints have been enforced on the initial population. Some of these constraints were imposed to make sure the resulting wells are drillable, while others are put in place to avoid creating solutions that are known to perform poorly due to violating common engineering practices. Considering that we have control in the initialization process, the constraints can be easily applied to the initial population. Nevertheless, reproduction might result in invalid solutions that we are continually filtering and excluding from evaluation. Some of the simpler constraints are:

- The minimum distance between any well and all other wells/segments must be more than 750' to mitigate well interference effects. This number was recommended by the reservoir management team for this field as it approximates the wells' drainage area.
- The maximum total length of each lateral cannot exceed 4000' to avoid swelling of shale layers. These layers in this field are known to swell if exposed to drilling fluids for long periods.
- The maximum possible Z<sub>h</sub> is set to 120' since the average net pay in the reservoir is 150'.
- To avoid lateral emanation from the end of the mainbore, angle difference between the two must be more than 30°. This angle, however, should not exceed 90° as obtuse angles between the lateral and mainbore are difficult to drill.

Considering an arbitrary property, P, initial properties relating to the last three constraints can be generated by the following equation:

$$P_{init} = P_{\min} + rand(0,1)(P_{\max} - P_{\min})$$
(3-4)

Other more complicated constraints will be explained in separate sections that will follow.

#### 3.3.1. Saturation Screening

During the early stages of this study, it was noticed that many individuals in the initial population produce minuscule amounts of oil. These individuals impaired the quality of the initial population and deterred the evolution process. Analyzing these individuals revealed that most of them were completed in very low oil saturation ( $S_o$ ) zones. This motivated us to screen for grid saturations that candidate individuals should reside in. The screening process can be considered as a rule-based constraint to avoid creating and simulating potentially known poor performers.

Inspecting the relative permeability curves in Figure 3-3 shows that the residual oil saturation (So<sub>r</sub>) is around 0.4. Yet, the initial oil saturation in 39% of the cells is below this relatively high So<sub>r</sub> value. An indexing system similar to the one developed by Bittencourt and Horne (1997) was applied to overcome this issue, where cells that do not contain moveable oil will be excluded from the well location initialization process. An example of this procedure is illustrated in Figure 3-4 for layer 4 (arbitrarily chosen) of the reservoir model. Green areas correspond to cells with an initial S<sub>o</sub> higher than So<sub>r</sub>, whereas red cells represent the other possibility.

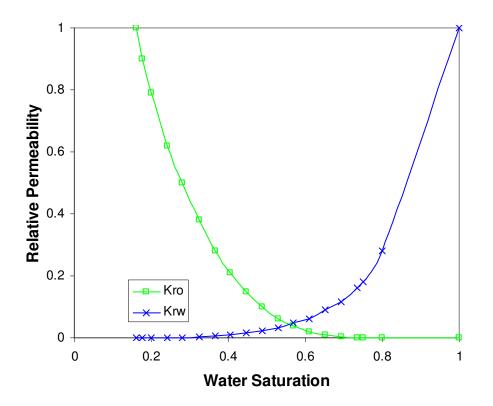


Figure 3-3: Oil and water relative permeability curves.

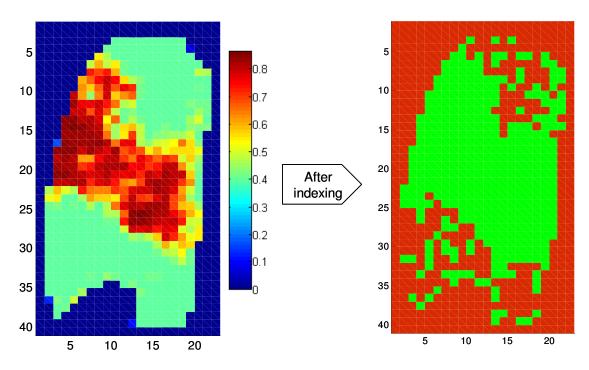


Figure 3-4: Implementing the indexing method on initial grid oil saturations.

The second step is to randomly select one of the green cells as the midpoint of the current well. Three random variables are then assigned to determine the relative x, y, and z positions within that cell. Once this procedure is completed, it is more likely that the well would be draining from a productive zone and assignment of the other variables can be done normally. Since the luxury of controlling well variables is not available during reproduction, a different precautionary step is taken at that stage in the optimization. A function is applied to all reproduced individuals before they are simulated to check for the average oil saturation in the producers' completion zones, which is determined by:

$$\overline{S_o} = \frac{1}{cell_{count}} \sum_{i=1}^{i=P_{num}} \sum_{j=1}^{j=lat_{num}} \sum_{k=1}^{k=cell_{num}} \sum_{k=1}^{cell} S_{o(i,j,k)}^{cell}$$
(3-5)

To test the effect of implementing this constraint, a case was designed with three deviated producers and two deviated injectors. The GA parameters were identical to those listed in Table 2-2 with the optimal  $P_{xo}$ ,  $P_{mut}$ , and  $f_{select}$  found in Section 2.4.1. Dynamic mutation was not used in this test and the three wells were produced under a rate control of 9 MBOD. Figure 3-5 compares results of the saturation screening function with the results of a standard run after running each case three times. After 600 simulations, applying the GA with screening for cells with movable oil predicts better results. The average cumulative production of the best solution for this method is around 10% better than that when no screening is used. The latter case might still reach better solutions if allowed to run longer but the evolution seems slower when compared to the other case with saturation screening for the same optimization duration.

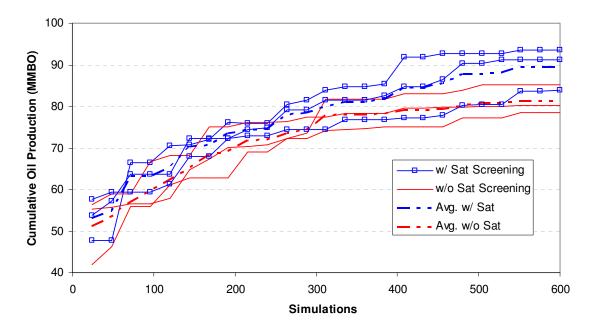


Figure 3-5: Fittest individual performance comparison averaged over three runs with and without the saturation screening method.

Despite the observed performance improvement, it is important to mention that more testing is needed to be conducted to find an optimum cut-off value for  $S_o$  or to formulate a more accurate proxy function to bypass some of the simulations. Usage of average saturation value is only a quick and simple way to characterize the productivity of the well. Generalization of Equation (3-5) can eliminate potential good solutions.

#### 3.3.2. Reservoir Boundaries

What has been described in the previous section only applies to producers' midpoint selection. With the random selection of well length and rotation angle, some manipulation had to be performed to keep the toe and heel points within the reservoir boundaries. This is especially true for the vertical boundaries, which are variant due to using different heights for each cell in the model. Horizontal limits, on the contrary, are constant. Moreover, using corner point grid makes this procedure more complicated and results in tilted planes as ceil and floor of the cells (Figure 3-6). In other words, any point in the xy-plane would carry different z-coordinate limits. The following procedure was followed to make sure the heel and toe points stay within the reservoir model.

- Once the three midpoint coordinates, well length, and the rotation angle are determined, calculate the x and y coordinates of the heel and toe.
- Devise plane formulas for the uppermost and lowermost planes bounding the (x, y) point calculated above according to the following equations (Wikipedia, 2009):

$$n_x x_{plane} + n_y y_{plane} + n_z z_{plane} + d = 0$$

$$d = -n \cdot p \qquad (3-6)$$

where nx, ny, and nz are the three components of an arbitrary vector, n, which is normal to the plane. p represents the coordinates of any point that belongs to the plane.

- Use these formulas to find maximum and minimum possible z-coordinates for the heel and toe.
- Set new limits for the variables  $Z_h$  honoring  $z_{min}$  and  $z_{max}$  from above.
- Randomly choose a Z<sub>h</sub> value for the well between its limits.

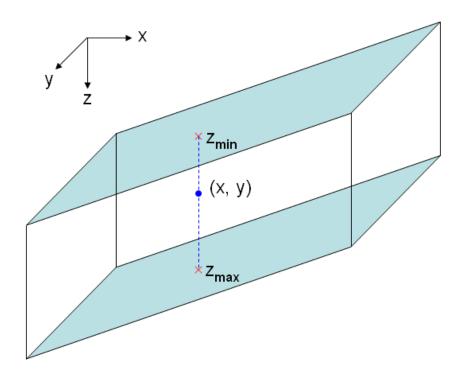


Figure 3-6: Setting well vertical limits within the irregular grid geometry.

#### 3.4. Preparing Input Files for the Reservoir Simulator and Reading Output Files

Once we are confident that all the individuals adhere to the constraints and can be passed to the simulator, simulation input files are written for each individual. When a particular scenario is being optimized, all reservoir model data are being held constant except for the well data, which change from an individual to another. These well data have to be put in a format that is readable by ECLIPSE. A MATLAB function was prepared to convert well coordinates into the corresponding I, J, and K cell parameters. From these data, the function prepares an include file containing all well design parameters specified by the WELSPECS, COMPDAT, WCONPROD, and WCONINJ keywords in ECLIPSE. When the simulation is finished, another function will read the resulting \*.RSM file to obtain production and injection data, from which an objective function is evaluated. Based on this objective function a ranking of the individuals takes place and the optimization continues.

#### 3.5. Objective Function Definition

One of the input parameters that the user has to define prior to submitting an optimization run is the type of objective function to be optimized. Two types are available in the formulation of this work: cumulative production and NPV. After each individual is simulated, calculation of each objective function is possible by reading the simulation output file. While cumulative oil production represents a single value, the total oil volume by the end of simulation; NPV takes more consideration of the economics of the project. The economic model we used is based on the work of Yeten (2003). NPV is calculated based on a fixed yearly effective discount rate as:

$$NPV = \left(\sum_{n=1}^{Y} \sum_{p=o,g,w} \frac{1}{(1+i)^n} Q_p^n \cdot C_p\right) - C_d \quad ,$$
(3-7)

where  $Q_p^n$  is the production rate of phase p during the year n,  $C_p$  is the unit profit or cost associated with this phase, and i is the annual percentage rate (APR), Y is the total number of discount years, and  $C_d$  is drilling and completion cost.  $C_d$  consists of several costs associated with the drilling operation and is given by:

$$C_{d} = \sum_{i=1}^{Well_{count}} C_{CAPEX} + L_{tot,i}C_{drill} + (Lat_{count} \cdot C_{mill}), \qquad (3-8)$$

where  $C_{CAPEX}$  is a capital expenditure cost per well including platform cost and the cost of drilling to the top of the reservoir,  $C_{drill}$  is the unit drilling cost per feet,  $C_{mill}$  is the cost of milling a new junction, and the rest of the variables are as defined previously.

#### 3.6. Other Implementation Issues

As a consequence of converting well coordinates from their real values to the corresponding simulator I, J, and K values, completions are assumed to be at the center of the grid blocks. As a result, straight well trajectories previously defined by the GA will be represented in a staircase manner when converted to the grid space. The error introduced by this phenomenon can be corrected by using the correct well index (WI) (Yeten, 2003). Due to the complex grid geometry in this model, a computation of the accurate WI could not be directly integrated into the optimization procedure and the default WI values given by ECLIPSE were used. The effects of overlooking this correction will be discussed in Section 4.4. Also, when the input well files were prepared for the simulator, it was assumed that all well segments are fully perforated. Selective perforation can be used by introducing new variables but it was not considered in this study.

Additionally, the technique for generation of the initial population can be improved. With inaccessibility to openhole logs and other field data, all individuals in this study were generated randomly. As more data become available, a well engineered initial solution can be constructed and fed to the GA for improvement, which should generate better final solutions (Emerick et al., 2009).

#### 3.7. Concluding Remarks

In this chapter, a description of the reservoir model, problem parameters, and problem constraints were presented. It was shown that applying some constraints that eliminate expected poor performers, such as initial oil saturation screening, considerably improved optimization results. A methodology for keeping the wells within reservoir limits via

planar geometry was also explained. Finally, this chapter detailed some of the important interaction steps between the optimizer and the reservoir model, such as the information exchange mechanism and objective function calculation.

Now that the overall optimization procedure is defined, we are ready to present the results of applying it to the S1 reservoir model in the next chapter.

# Chapter 4

# 4. Results and Discussion

After making a decision about the optimization algorithm and determining a reliable set of GA parameters in Chapter 2, we are now ready to proceed to the third stage of the study by applying the algorithm to the S1 reservoir model. The first step in this stage is to investigate the possibility of further empowerment of the algorithm by combining it with some helper tools. The resulting hybridized algorithm from this step was then run on the field to draw some conclusions on the optimal field development plan. The final step was to examine the reliability of obtained optimum solutions under different assumptions that were made prior to the optimization. It is of high interest to find out if these solutions remain superior had the assumptions not been made. This step involves an uncertainty propagation study on the effects of aquifer strength, an assessment of assuming a default WI for the wells, and an appraisal of any consequences caused by upscaling the original reservoir model.

Unless otherwise mentioned, the following optimization parameters were used in this chapter. All tests were performed with the GA parameters listed in Table 2-2 with  $P_{xo} = 0.8$ ,  $P_{mut}$  dynamically assigned, and  $f_{select} = 0.5$ . Additionally, all producers were simulated with a bottom-hole pressure (BHP) control of 1000 psig, which is above  $P_{bub}$ . Injectors were operated with a BHP of 2500 psig. The population size of each run was equal to the number of variables, which is calculated from Equation (3-3). The maximum generation was adjusted appropriately to accommodate the complexity of the problem according to the findings of section 2.4.3. Three runs were made to get a dependable average of the studied case. In few cases, one of the three runs was omitted due to abnormally low objective function value and a replacement run was performed. Depending on the considered study and the expected economic implications, the objective

function was alternated between cumulative oil production and the NPV of the project. The runs in this study were parallelized over 20 computer nodes.

#### 4.1. Helper Tools

One of the advantages of the GA mentioned earlier is the ability to hybridize them with different optimizers and helper tools. Some of these helper tools are designed to speed up the algorithm, while others focus on improving the final GA solutions. Some of the most commonly used tools in the literature are ANNs, the Hill Climber, and Rejuvenation. The first helper tool was not implemented as Rigot (2003) has found that the method requires substantial simulation time to train ANN in order to see plausible improvement in complex reservoir models. The other two functions were already tested by Yeten (2003) on a synthetic model and are duplicated in this work to find out how well the algorithm performs in real field applications. Results of their implementation are presented next.

#### 4.1.1. Rejuvenation

The basic concept of rejuvenation is quite simple; the best solutions encountered during the overall optimization are resurrected during some specified generation levels. Because these solutions might have belonged to generations older than the previous generations, they will be referred to as ancestors (Fichter, 2000). These ancestors might have been mutated in an unfavorable manner and bringing them back creates opportunities for better mating of the top individuals, and thus, better offspring.

Rejuvenation was tested by optimizing the location of three producers and two injectors, each having three laterals. It was applied by keeping a pool of a similar size to the population. This pool keeps track of the fittest individuals during the course of optimization and composes the new population every five generations. Mutation is still applied to all individuals except the fittest one, but no crossover is considered during this generation. This optimization case will be referred to as Case 1, whereas the Base Case was run normally without rejuvenation. Each case was run for three times and the average results are plotted in Figure 4-1. When comparing the outcome of the Base Case (blue

curve) with Case 1 (red curve), it can be concluded that rejuvenation did not introduce noticeable improvement to the objective function of the fittest individual. An explanation of this finding might be realized when looking at average objective function of all individuals within the generation shown in dashed lines of the same colors. Jumps in the average values are introduced by rejuvenation every five generations. These jumps are sometimes high enough to bring the average fitness of individuals within a population to a very close value of the fitness of the best individual in this population. This is an indication of the similarity and loss of diversity in the different solutions in the population, which weakens the evolution process of the GA.

Case 2 was designed to alleviate the aforesaid drawback of losing population diversity. Instead of composing the whole population by rejuvenation like in Case 1, only half of it was generated from ancestors in Case 2 while the other half was created by regular crossover. To put things into perspective, let us consider the fifth generation of both cases with a generation size of 100. In Case 1, this generation will entirely be populated with the top 100 individuals previously met in generations 1 to 4 (with mutation activated for the top 99 individuals). The same is true for only 50 individuals for Case 2 as the other 50 are delivered by crossover and mutation of the fittest 50 individuals in the previous generation. After running Case 2 for three times, this procedure (green curve in Figure 4-1) has again failed to show significant improvement in final results. This method only improves the average fitness of all individuals, which does not have any significance in terms of optimization results.

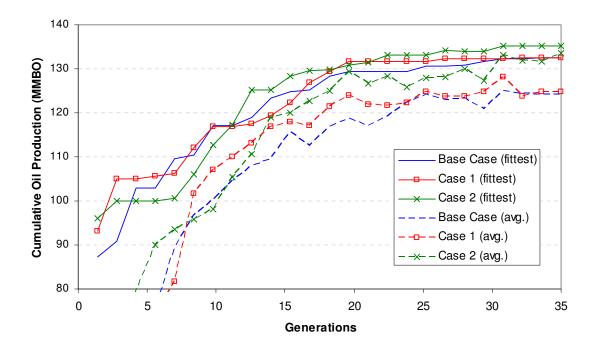


Figure 4-1: Fittest and average individual performance comparison averaged over three runs with different rejuvenation scenarios. Base Case: no rejuvenation applied. Case 1: rejuvenation applied to the whole population. Case 2: rejuvenation applied to half of the population.

#### 4.1.2. Hill Climber

The HC optimization method is a heuristic adaptation of the Hooke-Jeeves pattern search algorithm. As explained in the works of Reed and Marks II (1999) and Koza et al. (2003), the method is similar to GAs in being an evaluation-only search method, though it is more systematic and less random. Despite this, it is considered to be less applicable for complicated problems because it converges to local optima (also known as greedy algorithm) and because it starts with only one initial solution providing less exploration of the search space. The hill climbing procedure starts by taking a forward and backward step along one of the coordinates of the problem. A series of new steps are attempted in the direction that improves the objective function. Search within the current coordinate is halted when no further improvement is realized in this direction, after which, the next coordinate is tested. The greediness of the method arises from the fact that the search is only performed in the neighborhood of the initial guess with no information about other

areas of the objective function surface as demonstrated in Figure 4-2; a simple example for a function with two variables.

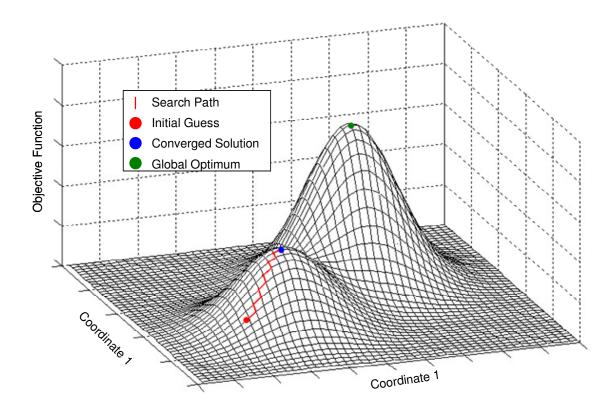


Figure 4-2: The hill climber's search pattern.

Nonetheless, blending GAs with the HC adds the missing exploration factor in the latter and helps to escape entrapment in local optima. At each generation level, the optimal solution found by the GA can be further improved by applying the HC, which excessively searches for improvement in the neighborhood of the solution found by the GA. The overall optimization process is now modified as depicted in Figure 4-3.

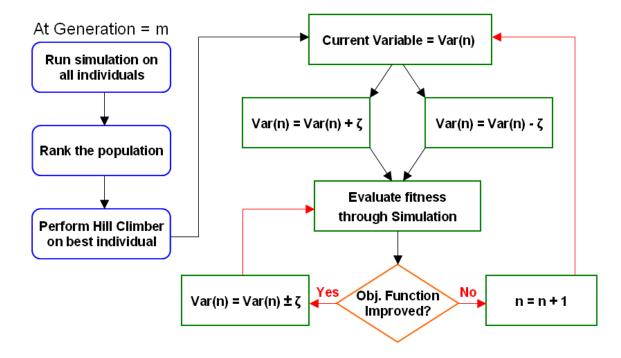


Figure 4-3: Flowchart of optimizing using genetic algorithms with the hill climber.

Four cases were tested to evaluate the benefits of adding the HC to the GA. The optimization problem studied comprises of two deviated producers and a deviated injector for all cases. The Base Case represents optimizing the problem with the GA alone. In Case 1, the HC was applied to the best individual of the initial population; while Case 2 executed the HC on the final solution given by the GA. Finally, the two algorithms were hybridized in Case 3; that is, the HC was run on the best individual that the GA found at each generation.

Results of the four cases are plotted in Figure 4-4. The benefit of the hybridized algorithm can be immediately recognized by the big improvement in Case 3 as compared with the Base Case. Since Case 3 combines both algorithms, we are interested in quantifying how much of the improvement is credited to each algorithm. Starting from the initial population, the HC by itself (Case 1) was able to improve the solution by around 20%. This improvement was achieved by the GA alone (Base Case) in about ten generations. When the HC was applied at the end of the base case, an improvement of 6% was

attained. This improvement is smaller in percentage when compared to Case 1 because the starting solution is already an optimized solution. Case 2, however, did not take the solution to the same level of Case 3. Another way to quantify the benefit of including the HC is to look at percentage improvement from one generation to the next. This calculation was performed on the Base Case and Case 3 and is shown in Figure 4-5. Juxtaposition of the two curves shows that most of the impact of the HC is at the early generations. After the tenth generation, the rate of improvement in the two cases is similar. In order, the final average objective function values of the fittest individual for the four cases are: 71.6, 64.0, 75.9, and 80.1 MMBO.

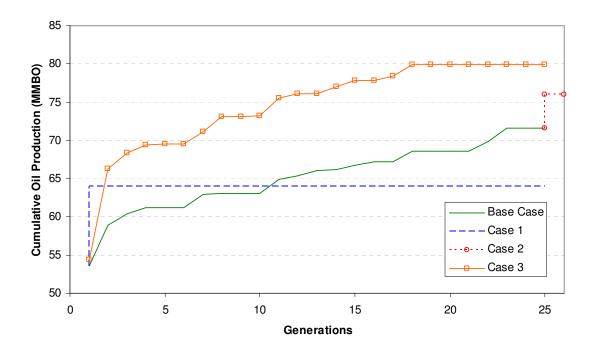


Figure 4-4: Fittest individual performance comparison averaged over three runs for different hill climber scenarios. Base Case: GA was run alone. Case 1: HC was run alone. Case 2: HC run at the end of GA. Case 3: Both algorithms run concurrently.

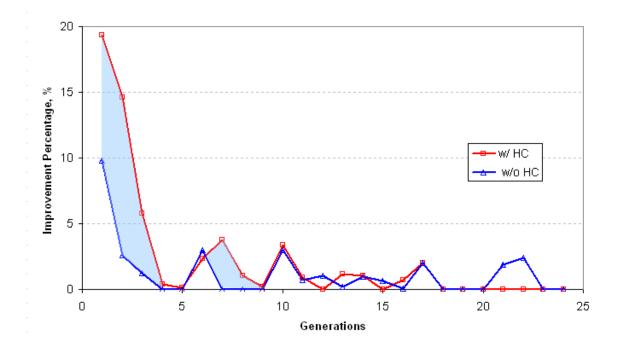


Figure 4-5: Percentage improvement in the objective function over previous generation with and without the HC

#### 4.2. Number of Laterals

This case aims to assess the sensitivity of the objective function to the number of laterals in each well. It can be used as a quick screening test to evaluate the performance of each well configuration and show the incremental value of adding more laterals. To achieve this, the locations of three deviated producers and two deviated injectors were optimized first. Then, we proceed by adding one lateral to each well until the fourth lateral is reached. Optimization parameters are as described in this chapter's introduction with cumulative oil production as the objective function. The HC was activated for the first ten generations in each run.

Results for the five optimization cases averaged over three runs are presented in Figure 4-6. As expected, the more the laterals in the well, the more cumulative oil is produced. However, the difference was marginal in some cases and it is also important to address if recovering the extra amount of oil is worth the associated increase in investment from drilling costs. For that purpose, the optimization was rerun after changing the objective

function to the projects' NPV as described in Section 3.5. The economic parameters are best estimates of the average costs and profits for the crude grade and field location and are listed in Table 4-1. Results of this run are plotted in Figure 4-7, which shows a similar trend to the results of Figure 4-6. This pattern was only broken when the forth lateral was added, which makes us question the value of drilling a quad-lateral well in the field.

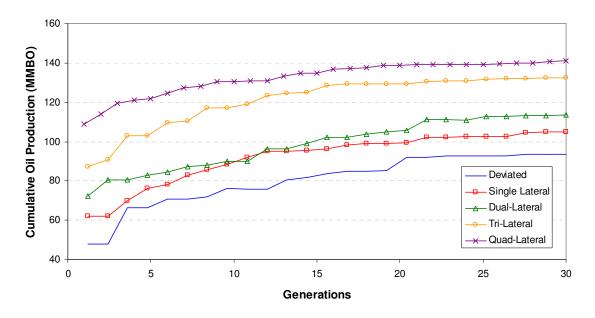


Figure 4-6: Cumulative oil production of the fittest individual averaged over three runs when using different number of laterals.

Table 4-1: Economic parameters used to calculate the NPV of the optimum lateral number study.

Economic Parameter	Value
Annual percentage rate, %	10
Oil selling price, \$/bbl	60
Water production cost, \$/bbl	3
Water injection cost, \$/bbl	3
C <sub>CAPEX</sub> , MM\$/well	1.5
C <sub>mill</sub> , MM\$/junction	1
C <sub>drill</sub> , \$/foot	800

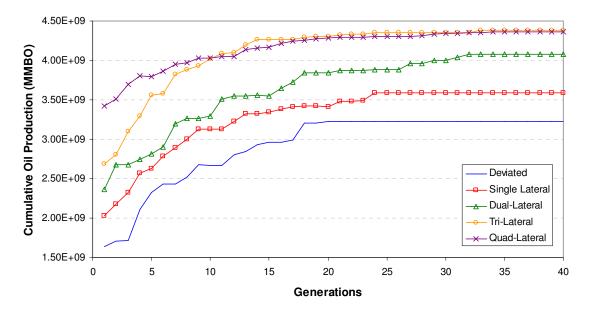


Figure 4-7: NPV of the fittest individual averaged over three runs when using different number of laterals.

It is worth mentioning that the resulting well locations from each run were considerably different with preference to particular regions that apparently have higher permeability. The difference is attributed to the stochastic search nature of the algorithm and the dissimilar initial population used for each run. The optimum well locations of each case can be viewed in Figure 4-8. Most of the scenarios gave a peripheral injection pattern.

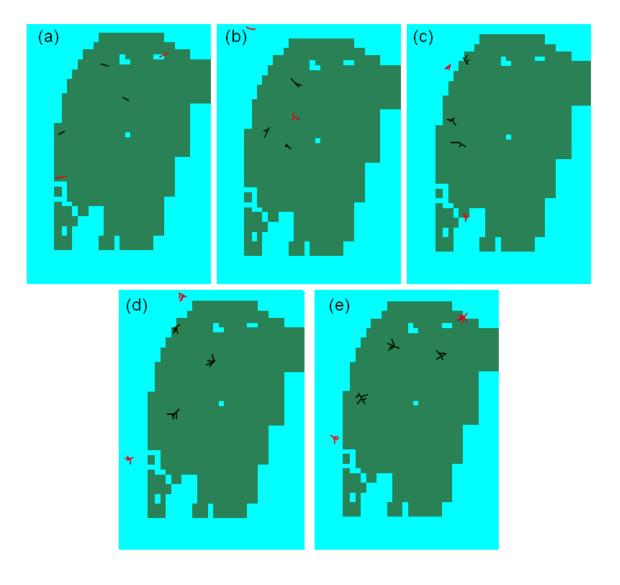


Figure 4-8: Optimum well locations for: a) Deviated, b) Single-lateral, c) Dual-lateral, d) Tri-lateral, and e) Quad-lateral wells.

## 4.3. Effects of Using Default Well Index

As previously mentioned in Section 3.4, solutions obtained from the GA are not represented in the exact manner by the reservoir simulator. While wells are represented as straight lines by the optimizer, the finite difference reservoir simulator represents as completions at the centers of grid blocks. The resulting difference in well length can be accounted for by using the correct WI for the wells instead of the default WI used in ECLIPSE (Yeten, 2003).

Several methods are available to calculate the WI. One of the most common methods to calculate the correct WI is the projection method. However, this approach requires cell faces to be parallel to the coordinates, which is not the case for this reservoir model (Shu, 2005). Another approach that provides the WI is a semi-analytical approach that calculates the index using well and block pressures using the following equation:

$$WI_i = \frac{q_i^{well} \mu}{\left(p_i - p_i^{well}\right)} \tag{4-1}$$

This approach is implemented by AdWell 2.2, a research simulator developed in Stanford (for detailed procedure description, refer to: Wolfsteiner et al., 2003).

With inaccessibility to the source code of the software, complete integration between WI correction and optimization could not be achieved. Instead, the effects of using the default WI was assessed by simulating a sample of five individuals twice; once with the default WI and again with the accurate WI from AdWell. The five individuals were chosen semirandomly for that exercise to include some of the top and middle performing individuals. Results of running these simulations are presented in Table 4-2. These results indicate that using the default WI increases each scenario's productivity by a factor of 4-6.25% in four of the cases and around 11% in one case. The effects appear to be relative; the best individuals when the default WI is used are still the best after implementing the accurate WI. Individual-3 suffered the highest change between the two WI methods. This difference occurred because the edges of the mainbore of Producer 3 in that individual barely touches three grid cells; yet, the simulator represented that well in four complete cells (Figure 4-9). This resulted in approximately 55% mismatch between the real length of this segment and the length used in the simulator.

Individual	Default WI	Accurate WI	Difference (%)
1	130.9	123.2	6.25
2	132.5	125.4	5.66
3	129.6	116.8	10.96
4	139.3	132.2	5.37
5	124.3	119.5	4.02

 Table 4-2: Comparing cumulative oil production results for five individuals when the default and the average WI were used.

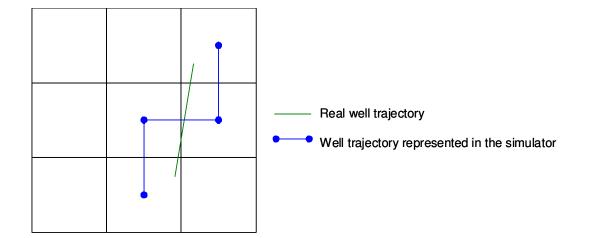


Figure 4-9: Comparing the trajectory of a well that returned high difference in cumulative oil production when the default and average WI were used.

### 4.4. Aquifer Uncertainty

Due to the imperfect knowledge of the reservoir geology, optimization is performed under a lot of uncertainties. Parameters that can greatly impact the optimization outcome include: rock and fluid properties, strength of the aquifer, and fluid contact depths. Uncertainty propagation can assess the effects of one or multiple parameters; the more parameters assessed, the more complicated the process. The variation in optimization results introduced by these uncertainties can play a key role in accepting or rejecting some of the optimized solutions. A lot of studies have attempted to study the effects of different geological inputs on well placement optimization outcome (Guyaguler, 2002; Yeten, 2003; Onwunalu, 2006). Because sufficient information was not available to assess the impact of other uncertainties, we choose to focus on a single source of uncertainty represented by aquifer strength. The aquifer in the model is represented numerically by increasing transmissibility over the oil-water contact. In addition to the default values, two runs were performed by increasing and decreasing this transmissibility value by 50%. The optimization involves three producers and two injectors each having three laterals. Since water production and injection is expected to change dramatically between the three scenarios, NPV was used as the objective function. The same individuals were used as initial population for the three cases to restrain its effects and the runs were repeated three times.

Results of each case are shown in Figure 4-10. Changing aquifer strength by 50% in each direction corresponded to a change of 5% in the NPV value (\$220 million) after ten years of simulation. Aquifer strength effect on final well positions for each run (Figure 4-11) was not as obvious. The injectors' location in the strong aquifer case is the only exception from this pattern, which is reasonable since short distance between injectors and producers coupled with a strong aquifer could lead to premature water production. Despite the above mentioned similarity, there was no relation in well and lateral trajectories from the three runs (examples of which are shown in zoomed-in boxes).

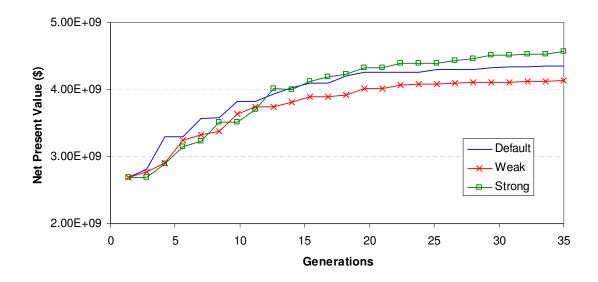


Figure 4-10: Fittest individual NPV comparison averaged over three runs when running the optimization with default, weak, and strong aquifer strength values.

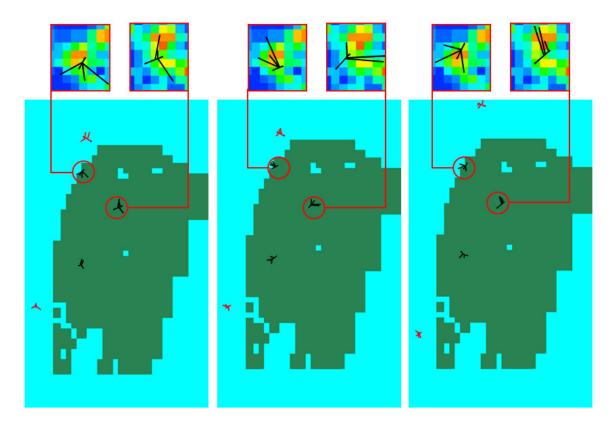


Figure 4-11: Final well location and design for the weak, default, and strong aquifer strength values.

However, these results are subject to projected economic model parameters used; namely, oil price and water injection and processing cost. The significance of this statement is illustrated by Figure 4-12, where we plot cumulative oil production and the water cut (WC) for the fittest individual in each case. Stronger aquifer resulted in more oil production but it also expedited the water break-through time (the WC exceeded 1% one year earlier than the medium aquifer value and two years before the weak aquifer). However, produced water did not exceed the field water-oil ratio constraint of 50% in any of the cases (Vohra, 2009).

To examine the combined effect of the strength of aquifer and uncertain economic parameters, the test matrix listed in Table 4-3 was generated by choosing two values for oil and water price for each aquifer strength. Five of the fittest individuals were chosen and simulations were run on them for each of the resulting 12 cases. For each solution, a more informed decision can be deduced after looking at the mean, which indicates the expected value of the solution; and the standard deviation for each individual, which quantifies uncertainty in aquifer strength and economic parameters. The evaluation criteria also depends on the adopted risk attitude. A risk averse (RA) attitude seeks to minimize risk, while a risk seeking (RS) attitude is on the contrary. A risk neutral (RN) attitude is somewhere in between the two. The fitness function for an individual can be found for each attitude as defined by Yeten (2003):

$$F = \begin{cases} f + \sigma \\ f \\ f - \sigma \end{cases}$$
(4-2)

where f is the mean and  $\sigma$  is the standard deviation.

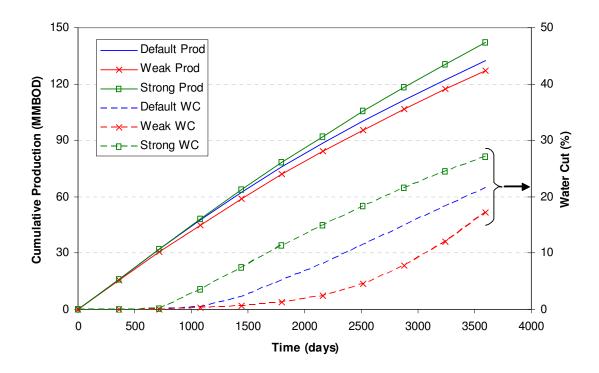


Figure 4-12: Cumulative oil production and water cut for the optimal solutions of the weak, default, and strong aquifer strength values

Results of completing the risk analysis procedure on the same individuals for the three aquifer values are listed in Table 4-4. The numbers show that Indivisual-2 consistently performs lower than the other wells (ranked bottom in 9 out of 12 cases). This individual retains the lowest objective function regardless of the risk attitude taken. Individual-1 is the best performer when weak and medium aquifer strengths are used. When aquifer strength is increased further, the higher resulting water production for this individual affects its objective function and Individual-4 becomes the fittest individual. This analysis advises us to choose Individual-1 if we opt either a RN or RA attitude and Individual-4 if a RS attitude is desired. Again, these two individuals are similar location wise but their laterals' orientation is irrelevant.

Case	Aquifer Strength	Oil Price (\$/STB)	Water Inj/Prod Cost (\$/BBL)
1	Weak	50	3.5
2		60	3.5
3		50	2.5
4		60	2.5
5	Medium	50	3.5
6		60	3.5
7		50	2.5
8		60	2.5
9	Strong	50	3.5
10		60	3.5
11		50	2.5
12		60	2.5

Table 4-3: Economic parameters chosen to test the effect of oil and water prices.

 Table 4-4: Objective function results (from Equation 4-2) after performing aquifer uncertainty risk analysis on five individuals.

Individual Case	1	2	3	4	5
1	3.41	3.30	3.30	3.32	3.21
2	4.25	4.11	4.12	4.15	4.07
3	3.46	3.34	3.35	3.38	3.34
4	4.29	4.14	4.16	4.21	4.20
5	3.45	3.33	3.39	3.41	3.32
6	4.30	4.15	4.22	4.26	4.20
7	3.50	3.37	3.43	3.47	3.45
8	4.35	4.19	4.27	4.32	4.33
9	3.37	3.35	3.44	3.47	3.39
10	4.22	4.17	4.28	4.33	4.29
11	3.42	3.39	3.48	3.53	3.53
12	4.27	4.21	4.33	4.39	4.43
f	3.86	3.75	3.81	3.86	3.81
σ	0.44	0.43	0.44	0.45	0.47
<b>F</b> ( <b>RS</b> )	4.301	4.180	4.253	4.304	4.287
<b>F</b> ( <b>RN</b> )	3.858	3.753	3.814	3.855	3.813
F (RA)	3.414	3.327	3.375	3.406	3.339

#### 4.5. Results of the Fine Model

Using the upscaled model in previous sections allowed us to conduct several tests to evaluate the optimization algorithm within a reasonable time. If the fine model was to be used instead, optimization time would increase by approximately 40-fold. Time limitations in reservoir management would not always tolerate such a long period of time before making a decision. However, it is still important to see if solutions obtained from the upscaled model are viable ones when the fine model is used, which is the main objective of this section.

The initial solution for this optimization will be composed from the multiple solutions already obtained from previous runs. All of these individuals have three producers and two injectors with three laterals. In addition to the top solutions, a number of mediocre solutions were added to the population to maintain its diversity. As this population is yet to go through any reproduction, it is easy to compare how well its individuals perform in the two models. Figure 4-13 demonstrates this comparison for 10 out of 30 individuals chosen for the initial population. These ten individuals were selected to maintain the distribution of good and mediocre solutions from the initial population. Although most individuals that performed well in the coarse model are still considered good solutions for the fine model, the plot clearly shows that well performance ranking is not preserved in the two models. The upscaled model tends to result in higher cumulative production with Individuals G and H being the only exception. Since the coarse model was obtained by single-phase upscaling, these discrepancies might be addressed by applying near-well upscaling.

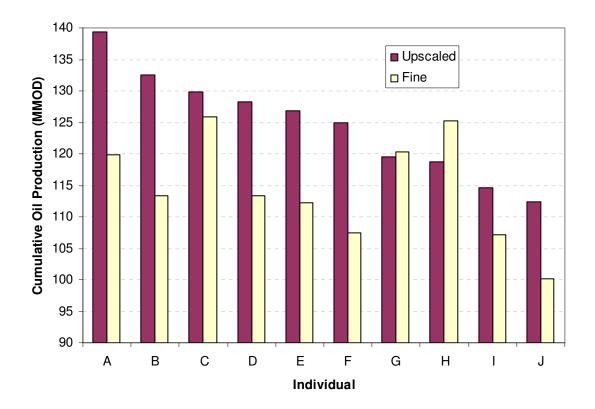


Figure 4-13: Individual performance comparison between the fine and upscaled model.

Once the initial population was in place, optimization was run for 25 generations and was repeated twice using the same initial population. The HC was applied to the first five generations. The evolution of the objective function can be seen in Figure 4-14. Unlike most other runs, percentage difference in the objective function value between the initial and final solutions is relatively small (around 10%) due to the high fitness of the initial population. Best solutions from each model are depicted in Figure 4-15 to provide a comparison of resulting well locations. As expected, and initially indicated by Figure 4-13, the best wells in the fine model assumed different locations from the best solution in the coarse model (Individual A). These positions are, however, close to those of Individual C with some differences in lateral orientation.

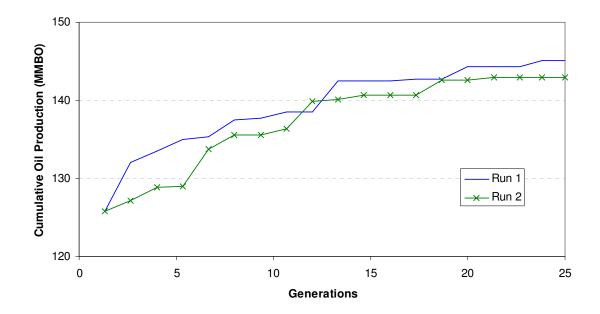


Figure 4-14: Objective function evolution of the fittest individual for the fine model after two optimization runs. The initial population for this optimization composed from the fittest individuals from the upscaled model.

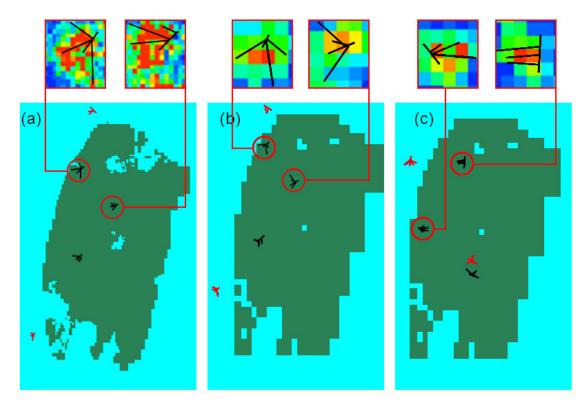


Figure 4-15: Comparison of well locations between: a) best individual in the fine model, b) Individual C from the coarse model (ranked 3<sup>rd</sup> in the coarse model but has similar locations to the individual in a), and c) best overall individual from the coarse model.

### 4.6. Concluding Remarks

This chapter focused on obtaining an optimum field development plan in terms of well locations and design by applying the cGA to the S1 reservoir model. Completing this exercise showed that the HC (Hill Climber) had a positive impact on the optimization results especially at the early stages. Running the cGA with rejuvenation, another helper tool, did not influence the performance of the algorithm for the tested case. By applying the hybridized algorithm to this reservoir, it was found that a tri-lateral well is the most cost efficient option as it had higher NPV than other tested well configurations. After a base case optimum scenario was reached, uncertainty and sensitivity studies were performed on this scenario to assess the effects of the aquifer strength, the used WI value, and the upscaling procedure. Solutions showed little sensitivity to the first two cases but the upscaling procedure seemed to affect the order of top solutions. A more

comprehensive summary of the results and conclusions of the whole study follows in the next chapter.

## **Chapter 5**

## 5. Conclusions and Future Work

### 5.1. Summary and Conclusions

With the challenging economic situations around the world, there is an ever growing demand to examine new tools to effectively manage oil reservoirs. A challenging aspect of reservoir management involves the optimization of nonconventional well location and design. Cost and productivity benefits from these wells can only be realized by efficient placement. This problem was researched in this work by comparing the performance of binary and continuous genetic algorithms in the S1 reservoir; a carbonate reservoir in Saudi Arabia. The optimization code was built in a way that could handle irregular grid shapes that are common in real fields. After performing sensitivity tests on the algorithm, optimum parameters were selected and more in-depth analysis was performed to reach an optimum field development plan. In addition, the effects of assuming a default WI for the well, using an upscaled reservoir model and optimizing under uncertain aquifer strength were assessed. The major findings and conclusions from this work are:

- Both GA types (binary and continuous) were applied to the same problem. Average results from the cGA were slightly higher and this algorithm appeared to be more consistent when several runs were made. The reproduction and overall optimization time was shorter in the cGA.
- Sensitivity analysis of cGA parameters revealed that early generations favor low mutation probability, while late generations favor medium values. Dynamic mutation was implemented to use the better mutation probability at the appropriate generation level. This analysis also showed that better optimization results can be obtained within a shorter period of time when dynamic population sizes are utilized.

- Applying an initial oil saturation constraint for producers' midpoints tends to reduce the number of poor individuals in the initial population, which eventually improves the objective function values.
- The use of the HC helper tool with the GA delivered fitter final solutions. It was found that complete hybridization of the two algorithms is more beneficial than running one after the end of the other. Moreover, most of the improvement from this tool was achieved in early generations. In contrast, other helper tools like rejuvenation did not have a major impact on results.
- The effects of using the default WI were tested by simulating some individuals with that WI value, as well as the accurate WI calculated semi-analytically. This exercise showed the effects to be relatively small with the exception of one out of five cases. On the other four cases, the percentage change in the objective function between the two indices was almost constant at about 5%.
- A study of aquifer uncertainty showed that aquifer strength has an effect on the objective function of the project but lesser effect was experienced on the location of optimum solutions. Risk analysis was also performed to account for the effect of economic implications of this uncertainty. This investigation showed that the choice of solution would differ depending on the risk attitude.
- By running the optimization on the fine and coarse reservoir models, it was found that the fittest individuals are not necessarily in agreement in both models. These differences might be reduced by implementing near-wellbore upscaling.
- While well locations in general differed from one run to another, there was a tendency for producers and injectors to seek particular regions of the reservoirs. The orientation of the well laterals, on the other hand, appeared to be random. Generally speaking, the wells were arranged in a peripheral injection with a central production system.

### 5.2. Future Work

The following suggestions are proposed for further investigation and improvement of the nonconventional well placement optimization framework.

- The conclusions obtained are only applicable for this kind of problem and reservoir. In order to validate them for a more general case, more simulations with different reservoir types should be done. Additionally, models with different levels of grid refinement should be considered to assess their impact.
- Other promising optimization techniques, such as particle swarm optimization, should be tested on this model or on a model with similar complexity to provide comparisons on the performance of each method.
- This study only considered one uncertainty aspect. Future studies should solve the optimization problem under more uncertainties especially geological uncertainty.
- If a coarse model is to be used for optimization, near-wellbore upscaling should be considered to achieve a better match between fine and upscaled optimization results.
- With the advancement in smart fields technology, future studies should consider coupling optimization methods with real-time data acquisition to reach a more realistic optimum solution

# Nomenclature

### Abbreviations

ANN	artificial neural networks
APR	annual percentage rate
bGA	binary genetic algorithm
BHP	bottom-hole pressure
cGA	continuous genetic algorithm
GA	genetic algorithm
GOR	gas-oil ratio
GSP	general search pattern
НС	hill climber
MLW	multilateral well
MRC	maximum reservoir contact well
NPV	net present value
OOIP	original oil in place
WI	well index

## Symbols

В	formation volume factor
С	constraint
С	compressibility
F	objective function
f	fraction
i	index, interest rate
inj	injector
$J_p$	junction position

k	permeability
L	length
Ν	number, a randomly distributed number
n	normal vector, ranking of an individual
rand	random number
Р	probability, property
р	point
prod	producer
prod r	producer ranking scale factor
-	
r	ranking scale factor
r S	ranking scale factor saturation
r S T	ranking scale factor saturation temperature

## **Greek Symbols**

β	blending coefficient
Ω	search domain
μ	viscosity
σ	standard deviation
$\varphi$	porosity
θ	top-view rotation angle

## Subscripts

CAPEX	capital expenditure
d	drilling
F	father
8	gas
i	index

М	mother
max	maximum
mill	milling
min	minimum
mut	mutation
0	oil
p	phase
r	residual, rock, relative
res	reservoir
select	selection
tot	total
W	water
xo	crossover

## Superscripts

lat	lateral
mb	mainbore
well	well
*	average

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## **Appendix A: Code and Input File**

Implementation of the described optimization procedure in this work was made possible through modularization of a number of functions coded with MATLAB 7.7.0 software. Some of the functions were modified from Farshi's (2008) work and others were originated by the author. All functions are included in a CD as a part of this report. In addition, the input file that enables the user to select important optimization parameters is included. A description of each function can be found in 'readme.doc' in the main folder of the CD. A more elaborate discription and comments on the functionality of the modules can be obtained by accessing the individual function files.