

	FY86	FY87	FY88	FY89	FY90	FY91	FY92	FW 3	FY94	FY95	FY96
1,800-m-deep reservoir depth : ± 1,800 m temperature ± 250°C	Hydraulic fracturing created a man-made reservoir	Drilled HDR - 1 to 1,805 m communicated to the SKG - 2	Circulation test for 2 weeks Deepen HDR - 1 to 2,205 m Set PBR	Drilled HDR - 2 to 1,910 m Circulation test for 29 days 40 % 4.5 MW thermal	Drilled HDR - 3 to 1,907 m communicated to the SKG - 2	Circulation test for 90 days 78 % 8.5 MW thermal					
2,200-m-deep reservoir depth : ± 2,200 m temperature ± 270°C							Hydraulic fracturing created a man-made reservoir	Deepen HDR - 3 to 2,303 m communicated to the HDR - 1	Sidetracked & Deepen HDR - 2 communicated to the HDR - 1	Preliminary circulation test for 25 days 40% 8-9 MW thermal	Circulation test to reduce the flow impedance
	SKG-2	SKG-2 HDR-1	SKG-2 HDR-1	SKG-2 HDR-1 HDR-1	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3	SKG-2 HDR-1 HDR-2 HDR-3

Fig.2 History of the Hijiori HDR test site

PRELIMINARY CIRCULATION TEST IN 1995

In 1995, a short-term circulation test was conducted with an injection well HDR-1, and two production wells HDR-2 and HDR-3 (Sato et al., 1995). The purpose of the test was to evaluate the deeper reservoir characteristics for a long term circulation test and to improve the connectivity of the deeper reservoir between the injection well and production wells. The period of the test was from August 6 to 30. The injection and production flow rate is shown in Fig. 3(a)-(b). At the beginning of the test, water was injected under high pressure to improve the connectivity at a maximum flow rate of about 60 kg/s as shown in Fig. 3(a).

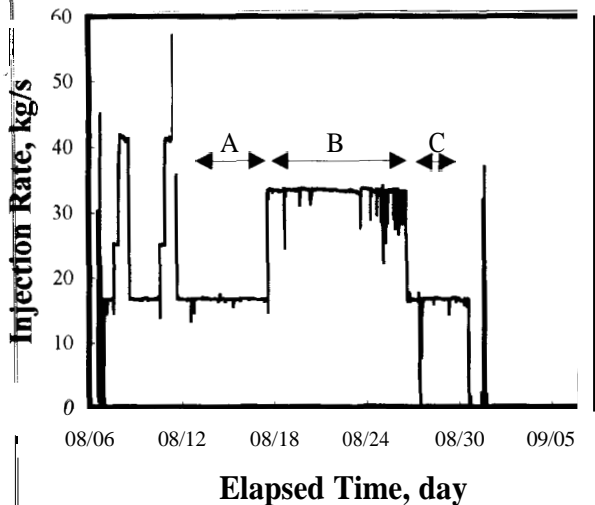


Fig. 3(a) Records of injection rate obtained during a preliminary circulation test in 1995

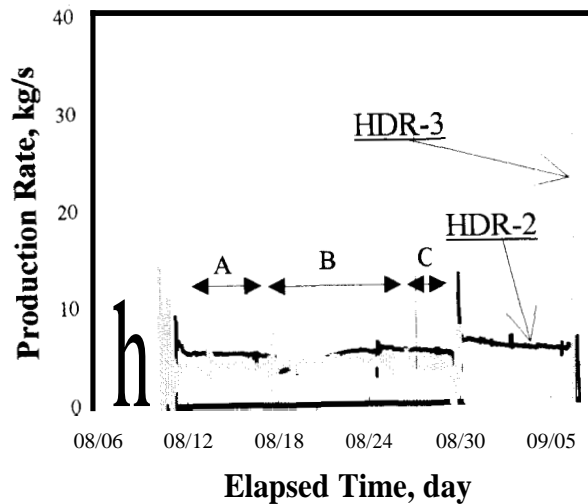


Fig. 3(b) Records of production rate obtained during a short-term circulation test in 1995

After initial high flow rate injection, the pumping was done at rate of 16.7kg/s(segment A and C) or 33.4 kg/s (segment B) during the test. As noted in Fig. 3(b), the mark of A, B and C indicate the period, when steam and hot water was produced from the two production wells. The result of these segments is shown in Table 1.

Productivity of two wells in segment A and segment C were almost equal. Production from HDR-2 was higher than that of HDR-3. The **summary** of the test is shown in Table 2. The total recovery rate of the test was about 40 %, and the amount of hot water and steam from HDR-2 was larger than that from HDR-3. Thus, we think that the productivity of HDR-2 was higher than that of HDR-3. But, the total production measured in wellhead

included the water loss from the shallow reservoir (Tenma et al., 1995). Therefore, we compare with the shallow reservoir and the deeper reservoir using data from several PTS (Pressure - Temperature - Spinner) logs.

Table 1. Production of HDR-2 and HDR-3 during a contact flow test of the preliminary circulation test in 1995

	Segment	A	B
Injection (HDR-1)	Flow Rate(kg/s)	16.7	33.4
	Total Flow(ton)	8565	25838
Production (HDR-2)	Steam (ton)	625	844
	Hot Water (ton)	2066	2939
	Recovery (%)	31.4	14.6
Production (HDR-3)	Steam (ton)	564	939
	Hot Water (ton)	1442	2368
	Recovery (%)	23.4	12.8

Table 2 Summary of short-term circulation test

Period	Aug. 6-30, 1995	25 day
Injection(HDR-1)	Total Flow (ton)	51500
Production (HDR-2)	Total production (ton)	13200
	Recovery (%)	25.6
Production (HDR-3)	Total production (ton)	6900
	Recovery (%)	13.4

COMPARISON BETWEEN THE SHALLOW RESERVOIR AND DEEPER RESERVOIR

As the Hijiori HDR system has two reservoirs, PTS logging was carried out to evaluate the characteristic of the deeper reservoir (Miyairi et al., 1996). Also, PTS logging was periodically conducted in 90-day circulation test, 1991. The pressure, temperature and flow rate were measured along the production well. Thus, we obtained pressure and flow rate from both the shallow and the deeper reservoirs.

Also, we calculated bottom-hole pressure of the injection well using the WBHT code (Cremer et al., 1979). In 90-day circulation test, bottom pressure calculated by WBHT and wellhead pressure are shown in Fig. 4. As shown in Fig. 4, bottom pressure is almost about 21 MPa. And we calculated bottom pressure of injection well in preliminary circulation test, too. Thus, the relationship

of differential pressure and flow rate measured using by PTS logging on both the shallow and the deeper reservoirs are shown in Fig. 5. Here we have differential pressure, we subtract measured pressure from calculated bottom pressure. In case of the shallow reservoir, we used data of the main fracture (Tenma et al., 1994). And, we used measured pressure at 1900 m depth in the deeper reservoir. The result are as follows.

- 1) The connectivity of main fracture of HDR-2 is almost equal to that of HDR-3 in the shallower reservoir.
- 2) In the case of the deeper reservoir, the connectivity of HDR-2 is higher than that of HDR-3.
- 3) the connectivity of the shallower reservoir is higher than that of the deeper reservoir.

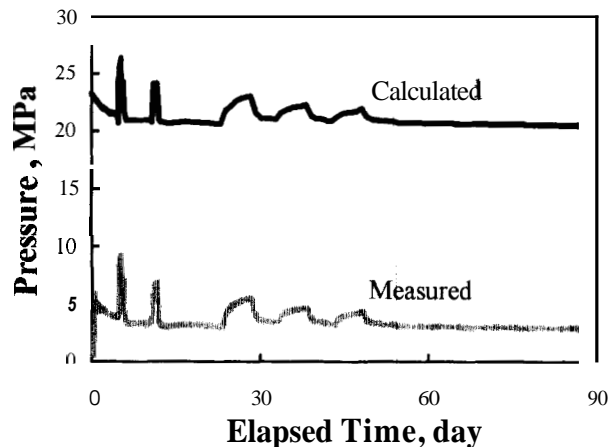


Fig. 4 History of calculated bottom pressure of Injection well (SKG-2) and measured pressure in 90-day circulation test, 1991

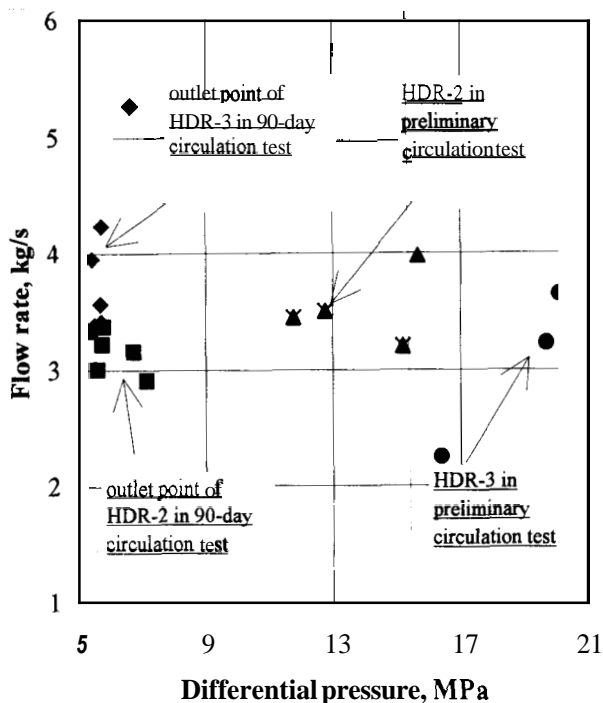


Fig. 5 Comparison with shallow reservoir and deeper reservoir

FUTURE TASK

In 1996, a one-month circulation test was carried out with HDR-1 as an injection well and HDR-3 as production well. The purpose of this test was to improve the connectivity of fractures between HDR-1 as the injection well and HDR-3 as the production well, because performance of both HDR-2 and HDR-3 were different. Data were obtained to evaluate the behavior of the deeper reservoir from these tests. Thus, we are planning a long-term circulation test of the Hijiori HDR system to confirm the feasibility of Hot Dry Rock power generation from the autumn of 2000 until the autumn of 2002.

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