

1 The Community Code Verification Exercise for
2 Simulating Sequences of Earthquakes and Aseismic Slip
3 (SEAS)

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Abstract

Numerical simulations of Sequences of Earthquakes and Aseismic Slip (SEAS) have made great progress over the past decades to address important questions in earthquake physics and fault mechanics. However, significant challenges in SEAS modeling remain in resolving multiscale interactions between aseismic fault slip, earthquake nucleation, and dynamic rupture; and understanding physical factors controlling observables such as seismicity and ground deformation. The increasing capability and complexity of SEAS modeling calls for extensive efforts to verify codes and advance these simulations with rigor, reproducibility, and broadened impact. In 2018, we initiated a community code-verification exercise for SEAS simulations, supported by the Southern California Earthquake Center (SCEC). Here we report the findings from our first two benchmark problems (BP1 and BP2), designed to test the capabilities of different computational methods in correctly solving a mathematically well-defined, basic problem in crustal faulting. These benchmarks are for a 2D antiplane problem, with a 1D planar vertical strike-slip fault obeying rate-and-state friction, embedded in a 2D homogeneous, linear elastic half-space. Sequences of quasi-dynamic earthquakes with periodic occurrences (BP1) or bimodal sizes (BP2) and their interactions with aseismic slip are simulated. The comparison of >70 simulation results from 11 groups using different numerical methods, uploaded to our online platform, show excellent agreements in long-term and coseismic evolution of fault properties. In BP1, we found that the truncated domain boundaries influence interseismic fault stressing, earthquake recurrence, and coseismic rupture process, and that agreement between models is only achieved with sufficiently large domain sizes. In BP2, we found that complexity of long-term fault behavior depends on how well important physical length scales related to spontaneous nucleation and rupture propagation are resolved. Poor numerical resolution can result in the generation of artificial complexity, impacting simulation results that are of potential interest for characterizing seismic hazard, such as earthquake size distributions, moment release, and earthquake recurrence times. These results inform the development of more advanced SEAS models, contributing to our further understanding of

Introduction and Motivation

When we develop models of physical systems, credible and reproducible results are essential to scientific progress. Robust predictive models of earthquake source processes have become important means for studying fundamental questions in earthquake science. Models of single earthquakes (known as *dynamic rupture simulations*) have emerged as powerful tools for understanding the influence of fault geometry, friction and prestress on rupture propagation, and for explaining observations of high-frequency ground motions and damage zones (Day, 1982; Olsen et al., 1997; Nielsen et al., 2000; Duan and Oglesby, 2006; Ripperger et al., 2007; Bhat et al., 2007; Dunham et al., 2011a,b; Lozos et al., 2011; Gabriel et al., 2012; Shi and Day, 2013; Kozdon and Dunham, 2013; Xu et al., 2015; Wollherr et al., 2018; Ma and Elbanna, 2019). Many of the codes used for these studies incorporate advanced features such as 3D domains and complex fault geometries, leading to very large problems for which rigorous convergence tests can be too computationally expensive. An alternative means for verifying model results are code comparisons made across the different modeling groups, using cell sizes at the limit of computational feasibility. Over the past decade, the SCEC/USGS Spontaneous Rupture Code Verification Project has made significant progress in using code comparison studies to provide confidence in model outcomes (Harris et al., 2009; Barall and Harris, 2015; Harris et al., 2018).

Although these dynamic rupture simulations have contributed greatly to our understanding of the physical factors that govern ground motion, they are limited to single-event scenarios with imposed artificial prestress conditions and *ad hoc* nucleation procedures. In order to understand earthquake source processes and how fault slip history influences subsequent events, it has been widely recognized that we need models that simulate behavior over multiple seismic events and the intervening periods of aseismic deformation. To address this need, models of Sequences of Earthquakes and Aseismic Slip (SEAS) have emerged that consider all phases of earthquake faulting, from slow tectonic loading to earthquake nucleation (under self-consistent prestress

68 conditions), propagation and termination. However, so far codes for SEAS simulations
69 remain untested. Inspired by the success of the SCEC/USGS Spontaneous Rupture
70 Code Verification Project, this paper describes the efforts of the SEAS initiative – a
71 SCEC (Southern California Earthquake Center) funded working group who has ini-
72 tiated the first code-verification study for earthquake sequence simulations. In this
73 paper, we present the initial benchmark problems and results from the code com-
74 parisons submitted to our online platform (<http://scecdata.usc.edu/cvws/seas/>).
75 Through these exercises, we aim to provide confidence in SEAS model outcomes, de-
76 termine best practices for improvement of accuracy and efficiency of SEAS simulations,
77 and provide other scientists strategies for verification during code development.

78 In SEAS models the goal is to capture the interplay of interseismic periods and
79 the associated aseismic fault slip that ultimately lead to earthquake nucleation and
80 earthquakes (dynamic rupture events) themselves, in an effort to understand which
81 physical factors control the full range of observables such as aseismic deformation, nu-
82 cleation locations of earthquakes, ground shaking during dynamic rupture, recurrence
83 times and magnitudes of major earthquakes, see Figure 1. These features distinguish
84 SEAS models from both dynamic rupture models which only consider single events,
85 and the so-called earthquake simulators (*Tullis et al., 2012*). Earthquake simulators
86 are capable of simulating seismicity patterns over millennium time scales in complex
87 fault network systems (*Richards-Dinger and Dieterich, 2012*) but are missing key phys-
88 ical features that could potentially dominate earthquake and fault interaction, such as
89 stress transfer generated by dynamic waves, aseismic slip within fault segments, and
90 inelastic responses.

91 SEAS modeling is not without significant challenges, due to the varying temporal
92 and spatial scales that characterize earthquake source behavior. For computational
93 efficiency the vast majority of SEAS models do not consider full dynamics during
94 earthquake rupture, but rather take a "quasi-dynamic" approach, where inertia is only
95 approximated (see section for further details). Computations are further complicated
96 when material heterogeneities, bulk inelastic responses and fault nonplanarity are in-

97 cluded. However, accounting for such complexity is widely recognized as crucial for
98 understanding the real Earth and predicting seismic hazards. Significant developments
99 in SEAS models over the past decade have incorporated some of these complexities and
100 connected model outcomes to geophysical observations. For example, seismological and
101 geodetic observations have been combined with modeling of coseismic and quasi-static
102 (aseismic) deformation to infer the spatial distribution of fault frictional properties
103 (*Johnson et al.*, 2006; *Barbot et al.*, 2009; *Mitsui and Hirahara*, 2011; *Dublanchet*
104 *et al.*, 2013; *Floyd et al.*, 2016; *Jiang and Fialko*, 2016), the decay rate of aftershocks
105 (*Perfettini and Avouac*, 2004, 2007), the role of tremor and slow slip (*Mele Veedu and*
106 *Barbot*, 2016; *Dublanchet*, 2017; *Luo and Ampuero*, 2017), and long-term models have
107 been used to reproduce characteristics of multiple and/or repeating events (*Chen and*
108 *Lapusta*, 2009; *Barbot et al.*, 2012). The framework of earthquake cycle modeling is
109 also adopted to explain geodetic and geologic data (*Meade et al.*, 2013; *Kaneko et al.*,
110 2011; *Wei et al.*, 2013, 2018), study subduction zones (*Hori et al.*, 2004; *van Dinther*
111 *et al.*, 2013; *Noda and Lapusta*, 2013; *Liu and Rice*, 2005, 2007; *Li and Liu*, 2016,
112 2017), collision zones (*Qiu et al.*, 2016; *Michel et al.*, 2017), and explore induced seis-
113 micity phenomena (*McClure and Horne*, 2011; *Dieterich et al.*, 2015), among many
114 applications.

115 While SEAS models are being used to explain, reproduce, and predict earthquake
116 behavior and other geophysical phenomena, a critical step must be to ensure that these
117 methodologies are accurate. The SEAS initiative is also taking the step to improve
118 and promote a new generation of verified numerical SEAS models that can simulate
119 much longer periods of earthquake activity than single-event dynamic rupture simula-
120 tions but with the same level of computational rigor, while incorporating qualitatively
121 different features such as (a) pre-, inter-, and post-seismic slip and the resulting stress
122 redistribution, (b) spontaneous earthquake nucleation, and (c) physical processes rele-
123 vant to long-term slip such as interseismic healing of the fault zone, viscoelasticity, and
124 fluid flow. Such SEAS models can provide physics-based approximations for larger-
125 scale and longer-term earthquake simulators. In addition they can inform the initial

126 conditions and nucleation procedures for dynamic rupture simulations, however our
127 vision for SEAS models is to develop them all to include full dynamic ruptures, cap-
128 turing the range of processes and heterogeneities known to be essential for realistic
129 ground motion modeling.

130 SEAS Modeling Challenges and Initial Bench- 131 mark Problems

132 Although the ultimate SEAS modeling framework would naturally include dynamic
133 rupture modeling, current methods for simulating SEAS problems require computa-
134 tional codes that are fundamentally different from those used in single-event dynamic
135 rupture simulations. The use of variable time stepping and possible switching between
136 different computational schemes is required in order to resolve sub-seconds to year-
137 long changes. The interaction between the highly nonlinear nature of the problems
138 and round-off errors can lead to model divergence. The need to distinguish between
139 legitimate solution differences due and improper choices of algorithm and modeling
140 procedures necessitates new and more suitable comparison metrics.

141 SEAS models are unique in that they cover a wide range of numerical method-
142 ologies and applications in earthquake science. Methods based on spectral bound-
143 ary integral formulations (BIEM) are efficient in solving for earthquake ruptures with
144 quasi-dynamic or full inertial effects (*Lapusta and Rice, 2003; Lapusta and Liu, 2009;*
145 *Jiang and Lapusta, 2016*). Methods based on the finite difference method (FDM)
146 or a hybrid finite element/spectral BIEM have been used to simulate quasi-dynamic
147 ruptures on faults with more complex bulk rheologies (*Erickson and Dunham, 2014;*
148 *Erickson et al., 2017; Allison and Dunham, 2018; Mckay et al., 2019; Abdelmeguid et al.,*
149 *2019*). Other SEAS modeling approaches include boundary element methods (BEM)
150 for simulating slow slip and tremor (e.g., *Tse and Rice, 1986; Rice and Tse, 1986; Ong*
151 *et al., 2019; Goswami and Barbot, 2018; Luo and Ampuero, 2011; Nakata et al., 2012;*

152 *Liu, 2013; Wei et al., 2013*), coupling faulting with fluid/heat transport and inelastic
153 dilatancy (*Segall and Bradley, 2012a*), effects of surface topography (*Ohtani and Hi-*
154 *rahara, 2015*), frictional heterogeneities (*Kato, 2016*) and viscoelastic response (*Kato,*
155 *2002; Lambert and Barbot, 2016; Barbot, 2018*). A spectral element method (SEM)
156 has also been developed for simulating fully dynamic earthquakes in a heterogeneous
157 bulk (*Kaneko et al., 2010*).

158 To verify the accuracy of SEAS models based on these different computational
159 methods, the SEAS group developed our first benchmark problem, BP1, to test the
160 capabilities of different computational methods in correctly solving a mathematically
161 well-defined problem in crustal faulting. The overall strategy of our benchmark exer-
162 cises is to produce robust results and maximize participation, with the goal of obtaining
163 agreements in resolving detailed fault slip history over a range of time scales. These
164 efforts required us to better understand the dependence of fault slip history on initial
165 conditions, model spin-up, fault properties, and friction laws. Given the complexity
166 of this task, it was important to start from the most basic problem and gradually
167 add model complexity. BP1 is a 2D antiplane problem, with a 1D planar vertical
168 strike-slip fault embedded in a 2D homogeneous, linear elastic half-space with a free
169 surface, see Figure 2. Full details of this benchmark (and subsequent benchmarks),
170 including governing equations and initial and fault interface conditions, are available
171 online on the SEAS platform (<http://scecddata.usc.edu/cvws/seas/index.html>).
172 We include some of the details on the friction law here, for clarity of important con-
173 cepts.

174 The fault is governed by rate- and state-dependent friction (*Dieterich, 1979; Ruina,*
175 *1983; Marone, 1998*) where shear stress on the fault τ is set equal to fault strength F ,
176 namely

$$177 \quad \tau = F(V, \theta), \quad (1)$$

178 where $\tau = \tau^0 + \tau^{\text{qs}} - \eta V$ is the sum of the prestress τ^0 , the shear stress due to quasi-
179 static deformation τ^{qs} , and the radiation damping term $-\eta V$ as approximation to

180 inertia (*Rice, 1993*). $\eta = \mu/2c_s$ is half the shear-wave impedance for shear wave speed
 181 $c_s = \sqrt{\mu/\rho}$, where μ is the elastic shear modulus and ρ is the material density. The
 182 fault strength $F = \sigma_n f(V, \theta)$, where V is the slip rate and θ is a state variable. σ_n is
 183 the effective normal stress on the fault. For this first benchmark problem we assume
 184 θ evolves according to the aging law

$$185 \quad \frac{d\theta}{dt} = 1 - \frac{V\theta}{L}, \quad (2)$$

186 where L is the critical slip distance. The friction coefficient f is given by a regularized
 187 formulation (*Lapusta et al., 2000*)

$$188 \quad f(V, \theta) = a \sinh^{-1} \left[\frac{V}{2V_0} \exp \left(\frac{f_0 + b \ln(V_0\theta/L)}{a} \right) \right] \quad (3)$$

189 for reference friction coefficient f_0 and reference slip rate V_0 . Depth-dependent fric-
 190 tional parameters a and b define a shallow seismogenic region with velocity-weakening
 191 (VW) friction and a deeper velocity-strengthening (VS) region, below which a rela-
 192 tive plate motion rate is imposed. A periodic sequence of spontaneous, quasi-dynamic
 193 earthquakes and slow slip are simulated in the model, see Figure 3a, where results
 194 from the BICycleE code (*Lapusta et al., 2000; Lapusta and Liu, 2009*) show slip con-
 195 tours plotted against fault depth in blue every 5 yr during interseismic loading and in
 196 red every 1 s during the coseismic phase. Over a 1200 year simulation period, approx-
 197 imately 13 events take place, nucleating at a depth of ~ 12 km, rupturing to a depth
 198 of ~ 18 km, and accumulating ~ 3 m of slip at the Earth’s surface. Model parameters
 199 used for the benchmark are given in Table 1.

200 A critical physical length scale present in this first benchmark problem, often re-
 201 ferred to as the process zone or cohesive zone Λ , describes the spatial region near the
 202 rupture front under which breakdown of fault resistance occurs, and shrinks as ruptures
 203 propagate faster (*Palmer and Rice, 1973*). For fault models governed by rate-and-state
 204 friction, the quasi-static process zone at a rupture speed of 0^+ , Λ_0 , can be estimated

(Day et al., 2005; Ampuero and Rubin, 2008; Perfettini and Ampuero, 2008) as

$$\Lambda_0 = C \frac{\mu L}{b\sigma_n}, \quad (4)$$

where C is a constant of order 1. Another characteristic length scale which has been shown to control model behavior is the critical nucleation size h^* , which governs the minimum extent of the rate-weakening region under which spontaneous nucleation may occur, (see Andrews, 1976a,b; Rubin and Ampuero, 2005; Ampuero and Rubin, 2008). For 2D problems, the critical nucleation size can be estimated for the aging law (with $0.5 < a/b < 1$) as

$$h^* = \frac{2}{\pi} \frac{\mu b L}{(b-a)^2 \sigma_n}. \quad (5)$$

A cell size of 50 m was used for BP1, resolving Λ_0 with approximately 6 grid points and h^* with approximately 40 grid points.

We developed the second benchmark BP2 that is similar to BP1 to explore the model resolution issues, which will be important in future benchmarks in 3D when computational efficiency demands a larger cell size. Complexity of event sizes and recurrence times is known to emerge through a reduction in the characteristic slip distance L (Lapusta and Rice, 2003; Mitsui and Hirahara, 2011; Wu and Chen, 2014; Kato, 2014; Barbot, 2019; Viesca, 2016a,b; Cattania, 2019). Thus BP2 is exactly the same as BP1 except that L is halved, resulting in bimodal sequences of full and partial ruptures of the velocity-weakening region (every large event is accompanied by a smaller event and the sequence repeats periodically). Besides aiming for agreements between different models, one main objective is to understand complexity in simulated events and how to deal with numerical resolution issues. A reduction in L corresponds to a reduction in the quasi-static process zone size Λ_0 . BP2 requests model outputs using a cell size of 25 m, 50 m, 100 m, 200 m, 300 m, 400 m and 800 m. The first three cases resolve Λ_0 with approximately 6, 3, and 1.7 grid points, and the other four cases do not resolve Λ_0 . Figures 3b-d show results from the BICycle code using a cell size of 25 m, 100 m and 200 m respectively. Small cell sizes of 25 m and 50 m (the latter is not

shown) show nearly indistinguishable, bimodal patterns of events nucleating at ~ 15 km depth, suggesting model convergence. A cell size of 100 m leads to a resolution issue where periodic behavior is observed, but the bimodal sequence of events is replaced by an alternating sequence of large, small and medium sized events. A cell size of 200 m, which does not resolve the process zone, reveals a loss of periodic behavior altogether in favor of a broad range of event sizes and nucleation locations.

Modeling Groups and Working Platforms

For these benchmark exercises, we have used two SCEC-funded workshops (hosted in April and November 2018, http://scecddata.usc.edu/cvws/seas/workshop_presentations.html) as open platforms for modelers to share and follow recent scientific progress in the field, discuss details in benchmark design/results, and collectively decide the directions of our future efforts, with considerable inputs from students and early career scientists. Over 10 modeling groups participated in these first two benchmarks; the details of the group members and different computational methods are summarized in Table . Note that the modeler name refers to the member of the modeling group who uploaded the data to the platform for simulations done by the group. It does not necessarily refer to the code author(s) - see the references in Table for authorship and code availability. For time-stepping schemes, the majority of groups used adaptive Runge-Kutta methods for both benchmark problems (the details of which can be found in the references listed in Table), with the exception of QDYN, which applies a Bulirsch-Stoer method for BP1, and BICycleE, which incorporates adaptive time-stepping based on stability conditions derived from the choice of constitutive relationship.

To facilitate the submission and comparison of simulation results, we established an online platform that provides access to community resources and supports the submission, storage, visualization, and comparison of benchmark results, see Figure 4. For our first benchmarks, we adopted a platform with similar functionality developed

259 for the SCEC dynamic rupture simulation group ([http://scecddata.usc.edu/cvws/
260 seas/](http://scecddata.usc.edu/cvws/seas/)). All modelers can upload and immediately plot time-series data to quickly
261 assess the overall agreements between models for the time evolution of fault slip, slip
262 rates and shear stress at representative locations on fault. We use the online platform
263 for preliminary model comparisons and analyze more detailed model observables to
264 verify these computational codes.

265 Model Comparisons and What We Learned

266 It is important to note that the problem descriptions for BP1 and BP2 consider a semi-
267 infinite half-space. Codes based on a volume discretization (FDM/FEM) therefore had
268 to make their own decisions regarding computational domain truncation and far-field
269 boundary conditions. The figures in the following sections contain labels generated
270 by the platform which state the model group name and correspond to results from a
271 particular model set-up. Some results are followed by the version corresponding to
272 an alternative set-up, e.g. **abrahams.3** corresponds to results from the **abrahams**
273 group with an increased computational domain size of $(L_x, L_z) = (400 \text{ km}, 200 \text{ km})$ and
274 a remote displacement boundary condition, see the lower right of Figure 4. We discuss
275 in the next sections the implications that these choices had on model comparisons.

276 Results from BP1

277 For the first benchmark problem, BP1, we found qualitative agreements in nucleation
278 sites, depth extent of rupture, and slip with depth similar to those exemplified by
279 the slip contours in Figure 3a. In Figure 5 we plot time series of local shear stress
280 and slip rates at mid-seismogenic depth ($z = 7.5 \text{ km}$) from BP1 over the first 700
281 years for different model results. Results from several BEM codes as well as codes
282 with volume discretization (**abrahams** and **kozdon** modeling groups) and varying
283 computational domain sizes are compared in Figure 5a-b. The legends indicate the
284 computational domain size and boundary condition. For BEM codes, HS refers to a

285 half-space, and $(L_z, \text{boundary condition})$ refers to computational domain depth and
286 boundary condition, where BC3 corresponds to a periodic boundary condition. For
287 codes with a volume discretization, $(L_x/L_z/\text{boundary condition})$, provides the com-
288 putational domain size used and BC1 and BC2 refers to a far-field free surface or a
289 far-field displacement boundary condition, respectively.

290 Figure 5(a-b) show model results from a BEM simulation (**liu**, in black) along with
291 four model results from volume discretization codes, revealing quantitative differences
292 in interevent times and peak values. Interevent times for different models range from
293 approximately 78.3 to 78.8 years over the whole 3000 year simulation period, leading
294 to model divergence at a near-constant rate. We found that these discrepancies were
295 caused by choices in domain truncation and boundary conditions. We were surprised
296 to find that far-field boundary condition type leads to quantitative differences in long-
297 term fault behavior for relatively small domains (revealed by the blue and orange
298 curves). This in part is due to small differences in the physical problem being solved
299 by implementations that use periodic or finite domain boundary conditions compared
300 to the spatial domain BEM methods which represent a truly infinite domain, and
301 therefore larger loading regions. The green and red curves show how the discrepancy
302 in long-term behavior among computational methodologies decreases as the physical
303 domain size is increased, suggesting convergence of results across the modeling groups.
304 Figure 5(c-d) shows comparisons of all models with $L_z > 160$ km, further illustrating
305 that excellent agreements between model results can be achieved with sufficiently large
306 domain sizes.

307 While computational domain size and boundary conditions can lead to model di-
308 vergence over the long term, the coseismic behavior of individual earthquake are qual-
309 itatively well reproduced by all models. In Figure 6 we show the time series of shear
310 stress evolution near the nucleation depth (12.5 km) and slip rate (at a mid-seismogenic
311 depth of 7.5 km) during the coseismic phase for the 8th event in the sequence from
312 Figure 5. We chose these plotting depths as they best illustrate model discrepancies,
313 with time series aligned relative to the rupture initiation time at the depth of 12.5

314 km. Peak values in slip rates at 7.5 km depth occur approximately 10 s later, and
315 co-seismic surface reflection phases are marked for all four plots with black arrows.
316 Figures 6(a-b) show results from models on relatively small computational domains,
317 revealing discrepancies in pre-rupture stress levels near the locked-creeping transition
318 due to differences in interseismic loading, and resultant coseismic rupture behavior, in-
319 cluding peak shear stress and rupture speeds as evidenced by rupture initiation times
320 of the direct and surface-reflection phases at depth of 7.5 km. Figures 6(c-d) illustrate
321 excellent agreements for model results on larger domains. The discrepancy of <1 MPa
322 in prestress levels at transitional depths does not result in pronounced difference in
323 fault slip rate evolution.

324 **Results from BP2**

325 For BP2 we suggested submissions of multiple models with different spatial resolutions
326 from each group, see Table . By design, models with a cell size/node spacing that does
327 not resolve critical length scales – process zone size and nucleation zone size defined in
328 (4) and (5) – would produce increased complexity in earthquake sequences, observed
329 previously (*Rice, 1993; Ben-Zion and Rice, 1997; Day et al., 2005; Lapusta and Liu,*
330 *2009*), and illustrated in the cumulative slip profiles in Figure 3(b-d).

331 While drastic differences in small event patterns arise for large cell sizes, we found
332 that with increasing resolution results converge to an alternating sequence of large
333 and small events among most models. Figure 7a shows the long term evolution of slip
334 rates at 9.6 km (near the bottom of the seismogenic zone and above the earthquake
335 initiation depth) for the best model results (with a cell size of 25 m and large compu-
336 tational domain sizes). We found that even models with similar cell/domain sizes tend
337 to produce results that are initially closely matching, but diverge over time, likely
338 due to accumulation of numerical round-off errors and differences in computational
339 techniques. However, if we zoom in on the tenth event in the sequence (gray bar in
340 Figure 7a), the time series of fault slip rates, aligned with respect to the start time of
341 seismic slip at the depth of 12 km within each model, show good agreements (Figure

342 7b). While small discrepancies exist in peak slip rates and early source complexity,
343 partly due to differences in interevent times, the models with the highest resolution
344 exhibit good agreements in their overall coseismic behavior despite their divergence in
345 the long term.

346 Figure 8 illustrates how model agreement is gradually lost with decreased model
347 resolution. For cell sizes of 25 m and 50 m, long-term stress evolution near the locked-
348 creeping transition is qualitatively similar for the three models shown and the offset
349 in the timing of earthquakes does not significantly affect coseismic behavior of major
350 events, as indicated by comparable coseismic stress drops. For large cell sizes of 100 m
351 and 200 m, not only is the time offset more random, but also coseismic stress drops and
352 event patterns vary between models. Numerical artifacts and different computational
353 techniques likely contribute to the divergence of simulation results.

354 In Figure 9 we plot the distribution of earthquake sizes, seismic moment release and
355 frequency-size relation for two groups of models (**jiang** and **cattania**) with increasing
356 cell sizes. For the 2D problem, we define earthquake size as moment release per length
357 for each event, $M = \int \mu s dz$, where shear modulus $\mu = c_s^2 \rho \approx 32$ GPa and s is total
358 coseismic slip over the cell. While better resolved models (cell sizes of 25 m and 50 m)
359 show excellent agreements between the two groups, models produce dramatically dif-
360 ferent earthquake statistics when cell size increases to 400 m, with the most significant
361 discrepancies in smaller earthquakes between the two models (Figure 9a). The distri-
362 bution of total seismic moment release, M_t , calculated as the sum of moment release
363 during all earthquakes within a certain magnitude range, also changes with cell sizes,
364 though in a similar manner for the two model groups (Figure 9b). Overall, models
365 with larger cell sizes tend to produce large earthquakes with reduced total moment;
366 part of the moment deficit is accommodated through many more smaller earthquakes
367 and the rest through additional aseismic slip. For example, the total moment release
368 through largest earthquakes in 400-m models is only half of that in 25-m models. These
369 results demonstrate that simulated small earthquakes are especially sensitive to model
370 resolution and large earthquake behavior can also be affected. In addition, Figure 9c

371 reveals how different simulations with poor resolution can produce similar power-law
372 features in frequency-size distributions over certain ranges of earthquake sizes, as a
373 result of numerical artifacts rather than well-resolved physics.

374 In Figure 10 we illustrate the effect of model resolution on the partition between
375 seismic and aseismic slip. Normalized seismic moment release R_s is plotted against
376 depth for several modeling groups, in solid lines for total seismic moment release and
377 dashed lines for seismic moment due to surface-breaching events. $R_s = 0$ implies
378 that all plate motion is accommodated by aseismic slip on the fault, while $R_s =$
379 1 means that all moment is released through earthquakes. A transitional zone in
380 this partitioning around $z = H$ and down to $z = H + h$ ($H = 15$ and $h = 3$ in
381 this exercise) is evidenced in the well-resolved models ($\Delta_z = 25, 50, 100$ m). The
382 poorly resolved models, however, illustrate model discrepancies in the seismic/aseismic
383 partitioning, with the near-surface slip budget being increasingly accommodated by
384 small earthquakes and aseismic slip with increased cell sizes.

385 In Figure 11 we show interevent times for large surface-breaching events for all
386 models and cell sizes, showing a strong agreement of ~ 110 years for a cell size of
387 25 m, with an increasing variability and discrepancies among models with increased
388 cell size. Although the range of earthquake recurrence intervals are highly dependent
389 on cell sizes, the median values across models with larger cell sizes do not significantly
390 deviate from the uniform recurrence intervals in well-resolved models. This suggests
391 that at least some observables in these models retain information of the true behavior
392 of physical models and the larger cell sizes can be viewed as a factor that leads to
393 increased modeling errors.

394 Conclusions and Perspectives

395 For the first two SEAS benchmarks we found that discrepancies among well-resolved
396 models were significantly influenced by computational domain size, with larger domains
397 yielding improvements in agreements, regardless of domain boundary conditions. Spin-

398 up periods (time required for system to be independent of initial conditions) for well-
399 resolved models was relatively short - approximately 2-3 events. Results on large
400 domains agree well initially but still diverge over time, which was not unexpected due
401 to accumulation of round-off errors and differences in computational techniques. For
402 BP2 we investigated model resolution and observed qualitative similarities of bimodal
403 events when the process zone was resolved by approximately 3 and 6 grid points,
404 suggesting model convergence. A failure to resolve this length scale however, can lead
405 to substantial differences in long-term fault behavior as well as earthquake statistics
406 relevant to seismic hazard, such as frequency-size distributions and interevent times.

407 Although our initial benchmarks have a simple setup, comparison of results for tens
408 of models have yielded some unexpected and important insights, affirming the impor-
409 tance of starting simple in a community code verification exercise. The results and
410 lessons from our initial benchmarks prepare us for future benchmark problems that
411 incrementally incorporate additional, potentially dominating physical factors, includ-
412 ing fully dynamic ruptures, coupling with fluids, multiple fault segments, nonplanar
413 fault geometries, and inelastic bulk constitutive behavior (e.g., *Segall and Rice, 1995*;
414 *Noda and Lapusta, 2010*; *Segall and Rice, 2006*; *Segall et al., 2010*; *Erickson et al.,*
415 *2017*; *Lambert and Barbot, 2016*; *Qiu et al., 2016*; *Barbot, 2018*; *Ong et al., 2019*). For
416 future verification exercises, we plan to address important issues in SEAS simulations,
417 such as 3D effects, heterogeneous fault frictional properties, and full dynamics, which
418 should advance the state-of-the-art computational capabilities in our field.

419 The goal of the SEAS initiative is to promote advanced models with robust physical
420 features—a large spectrum of rupture styles and patterns, including slow-slip events,
421 complex earthquake sequences, fluid effects, dynamic stress changes, and inelastic
422 deformation—that are currently missing in the large-scale, long-term earthquake sim-
423 ulator frameworks such as ViscoSim, RSQSIM, Virtual California, and ALLCAL (*Pol-*
424 *litz, 2012*; *Richards-Dinger and Dieterich, 2012*; *Sachs et al., 2012*; *Ward, 2012*). This
425 new generation of verified SEAS models will help determine the controlling physical
426 mechanisms of earthquake nucleation, propagation, and arrest. The community-wide

427 initiative would also provide incentives and new ideas to characterize modeling un-
428 certainty for the increasingly complex earthquake source models, an important step
429 in using physics-based models for the assessment of seismic hazard. Future valida-
430 tion efforts comparing physics-based models with geophysical observations will bridge
431 studies in paleoseismology, geodesy, and seismology to understand fault behavior over
432 multiple temporal and spatial scales.

433 **Data and Resources:** Our online platform ([http://scecddata.usc.edu/cvws/
434 seas/](http://scecddata.usc.edu/cvws/seas/)) is being developed and maintained by M.B. The data for local fault properties
435 are stored on the platform.

436 **Author Contributions:** B.A.E. and J.J. designed the benchmark problems, analyzed
437 model results, co-organized the workshops and co-wrote this article. M.B. developed
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442
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Table 1: Parameter values used in the benchmark problem

Parameter	Definition	Value, Units
ρ	density	2670 kg/m ³
c_s	shear wave speed	3.464 km/s
σ_n	effective normal stress on fault	50 MPa
a	rate-and-state parameter	variable (see Fig. 1)
b	rate-and-state parameter	variable (see Fig. 1)
L	critical slip distance	BP1: 0.008 m BP2: 0.004 m
V_p	plate rate	10 ⁻⁹ m/s
V_{init}	initial slip rate	10 ⁻⁹ m/s
V_0	reference slip rate	10 ⁻⁶ m/s
f_0	reference friction coefficient	0.6
H	depth extent of uniform VW region	15 km
h	width of VW-VS transition zone	3 km
W_f	width of rate-and-state fault	40 km
Δz	suggested cell sizes	BP1: 25 m BP2: 25 m, 50 m, 100 m, 200 m, 300 m, 400 m, 800 m
t_f	final simulation time	BP1: 3000 years BP2: 1200 years
L_z	depth of computational domain	<i>not specified</i>
L_x	off-fault distance of computational domain	<i>not specified</i>

Table 2: Details of participating SEAS codes and modeling groups.

Code Name	Type	Modeler Name & Group Members	References
SCycle	FDM	abrahams (Abrahams/ Allison/Dunham)	<i>Erickson and Dunham</i> (2014) <i>Allison and Dunham</i> (2018) https://github.com/kali-allison/SCycle
FDCycle	FDM	erickson (Erickson/Mckay)	<i>Erickson and Dunham</i> (2014) https://github.com/brittany-erickson/FDCycle
QDESDG	DG-FEM	kozdon (Kozdon)	https://github.com/jkozdon/QDESDG
Unicycle	BEM	barbot (Barbot)	<i>Barbot</i> (2019) http://bitbucket.org/sbarbot
FDRA	BEM	cattania (Cattania/Segall)	<i>Segall and Bradley</i> (2012b); <i>Bradley</i> (2014)
BICycle	BEM	jiang (Jiang) lambert (Lambert/Lapusta) xma (Ma/Elbanna)	<i>Lapusta et al.</i> (2000); <i>Lapusta and Liu</i> (2009)
QDYN	BEM	luo (Luo/Idini/ van den Ende/Ampuero)	<i>Luo and Ampuero</i> (2017) https://github.com/ydluo/qdyn
ESAM	BEM	liu (Liu) wei (Wei/Shi)	<i>Liu and Rice</i> (2007)

817 **List of Figure Captions:**

818 Figure 1: Ingredients and observables for SEAS (sequences of earthquakes and aseismic
819 slip) models. In a conceptual fault-zone model, earthquakes initiate at seismogenic
820 depths (red star) and rupture through the interseismically locked regions (gray), while
821 aseismic slip occurs in deeper and sometimes shallower regions (yellow). For numerical
822 models, given fault zone properties, computational simulations can reproduce long-
823 term fault locking and creep over years to decades, punctuated by dynamic earthquake
824 ruptures over seconds to minutes. Seismic shaking and aseismic deformation are typical
825 observables from the surface.

826 Figure 2: Our first SEAS benchmark is based on the model in *Rice* (1993), where a
827 planar fault is embedded in a homogeneous, linear elastic half-space with a free surface.
828 A vertical cross-section of the 3D setting is taken so that slip varies only with depth
829 and deformation is 2D antiplane strain. The fault is governed by rate-and-state friction

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836 Figure 3: Cumulative slip profiles plotted over a 1,200 year period in blue every 5 years
837 during interseismic loading and in red every second during quasi-dynamic rupture.
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839 BP2 with a cell size of 25 m, (c) BP2 with a cell size of 100 m and (d) BP2 with a cell
840 size of 200 m. Number of events also listed, where we define a seismic event to be one
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843 website. (Top right) Currently available benchmarks. (Bottom right) Examples of
844 BP1 model submissions.

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858 space solution **luo** is the same in (b) and (d) and serves as a reference. The surface
859 reflection phase is marked by a black arrow.

860 Figure 7: Comparison of best-resolved BP2 models (cell size of ~ 25 m). (a) Long-term
861 evolution of slip rates at depth of 9.6 km; (b) coseismic evolution of slip rates at the
862 depth of 9.6 km for the 10th large events in the sequence (marked in gray in (a)). Time
863 series are aligned relative to the rupture initiation time at the depth of 12 km in each
864 model.

865 Figure 8: Increasing discrepancy in BP2 models due to an increased cell size of (a)
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867 of 9.6 km during the first 600 years is shown for models from three groups (**abrahams**,
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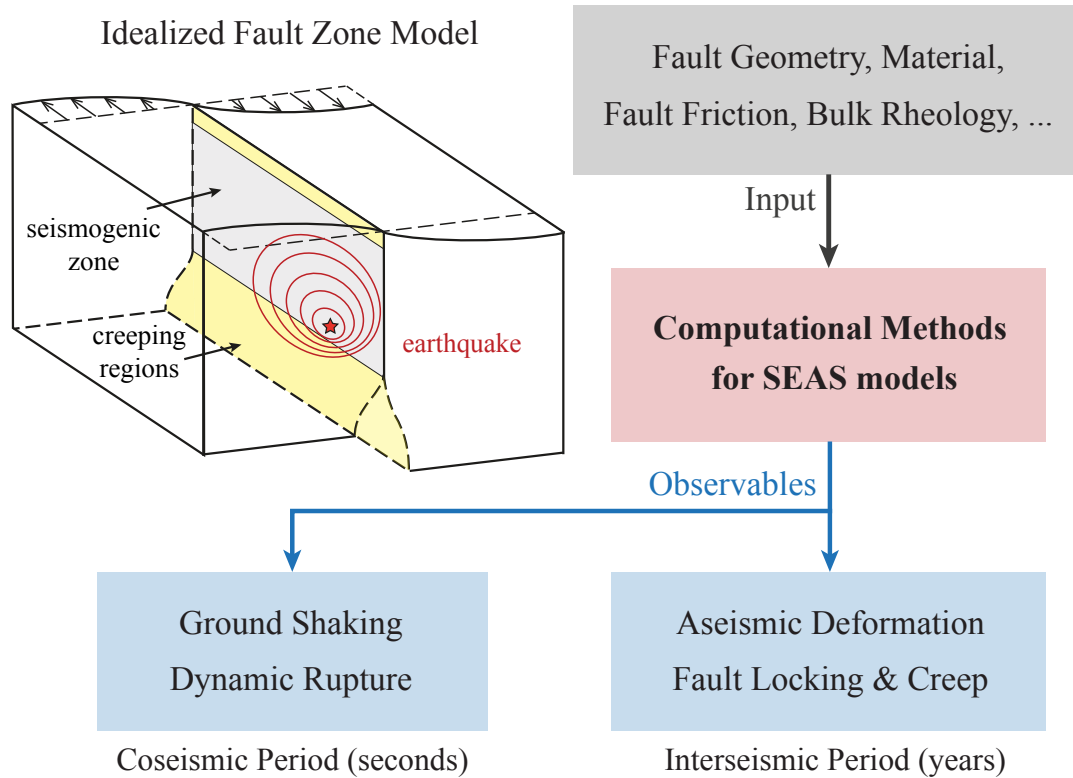


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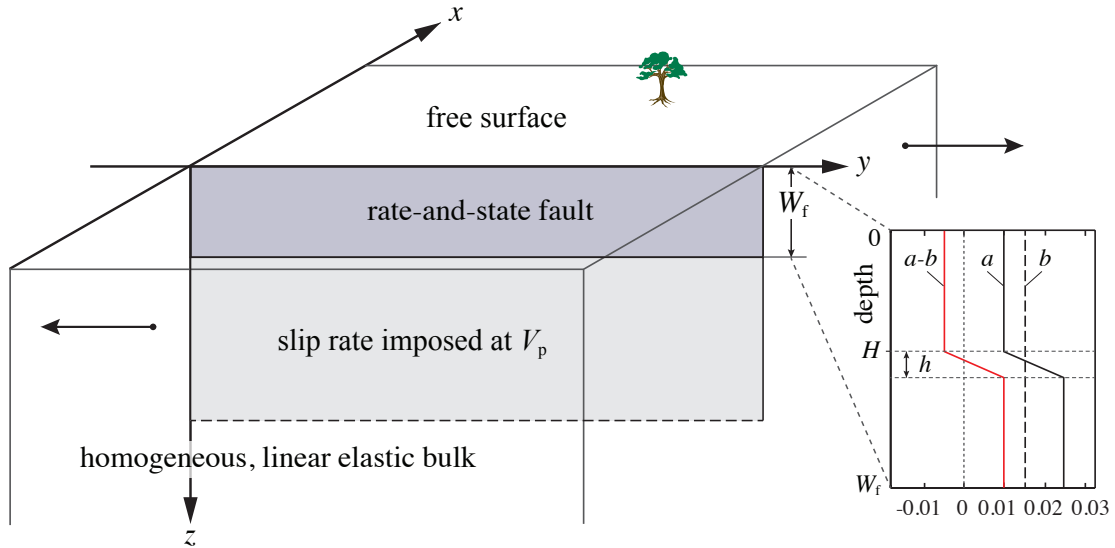


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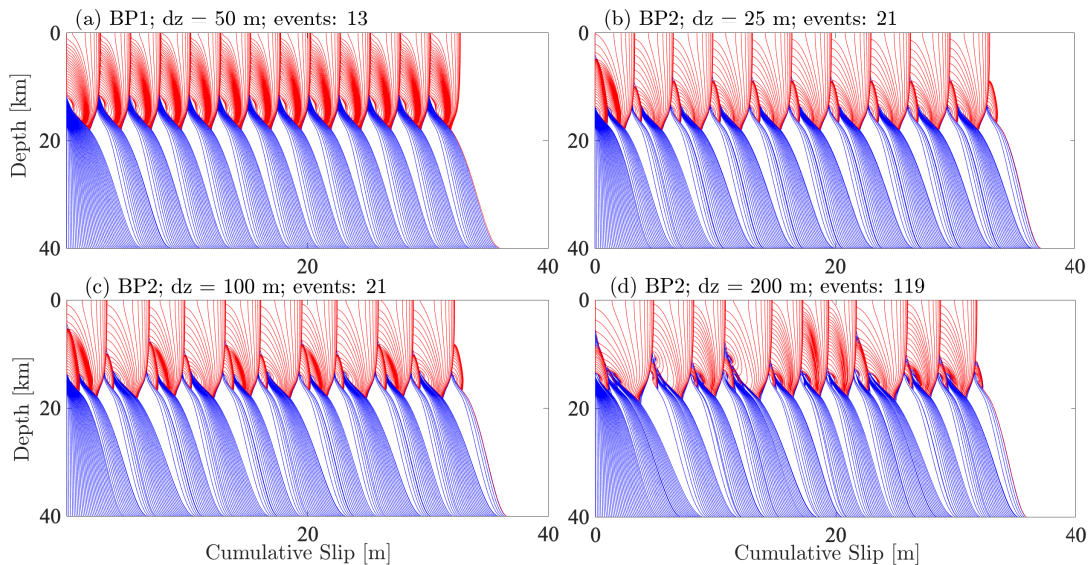



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The SCEC Sequences of Earthquakes and Aseismic Slip Project

[Benchmark Comparison Tool](#)

[Benchmark Descriptions](#)

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Benchmarks			
Name	Date	Description	Action
bp1	4/14/2018 8:08 AM	2D Antiplane Shear	Select
bp2	10/6/2018 6:20 AM	2D Antiplane Shear, Varying Cell Size	Select

Users			
		Select Checked	Select All
Name	Description		
<input type="checkbox"/>	abrahams	100 km X 80 km: Free surface outer BC	Select
<input type="checkbox"/>	abrahams.2	100 km X 80 km: Vp/2 outer BC	Select
<input type="checkbox"/>	abrahams.3	400 km X 200 km: Vp/2 outer BC	Select
<input type="checkbox"/>	barbot	Sylvain Barbot (Fortran90)	Select
<input type="checkbox"/>	barbot.2	Sylvain Barbot (Matlab)	Select
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<input type="checkbox"/>	cattania.2	Camilla Cattania - fdra (fft, 160 km)	Select
<input type="checkbox"/>	cattania.3	Camilla Cattania - fdra (fft, 640 km)	Select
<input type="checkbox"/>	erickson	Brittany Erickson	Select
<input type="checkbox"/>	erickson.2	Brittany Erickson	Select

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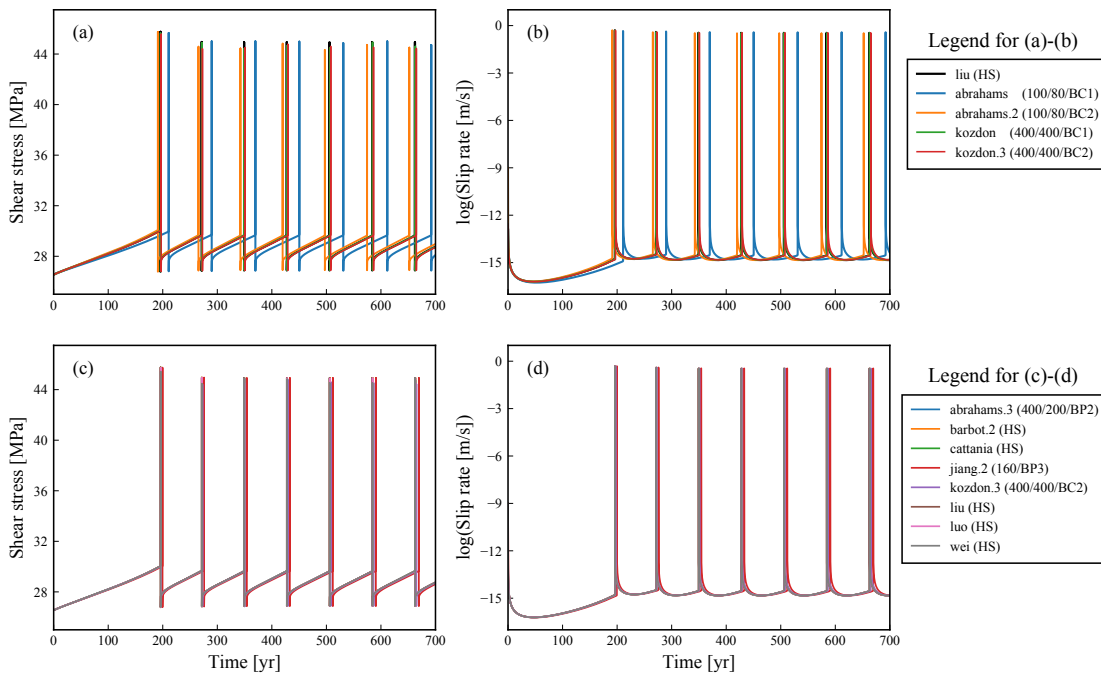


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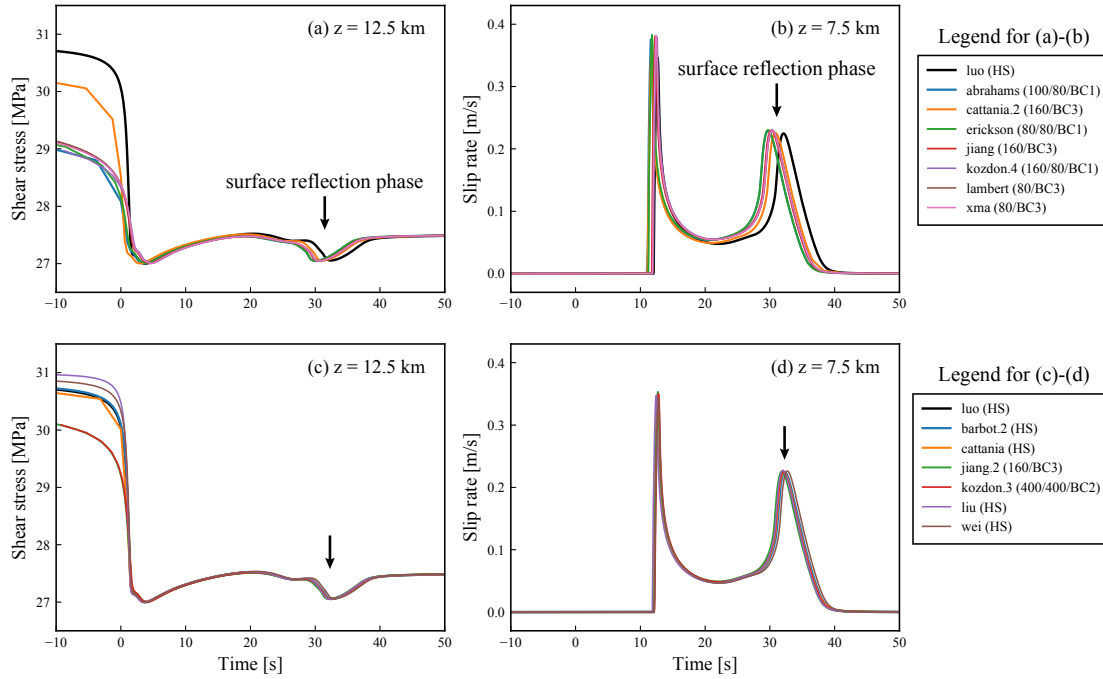


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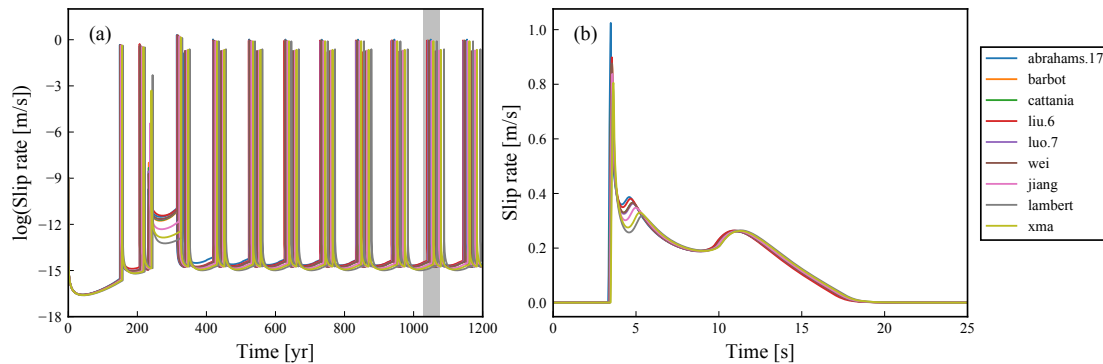


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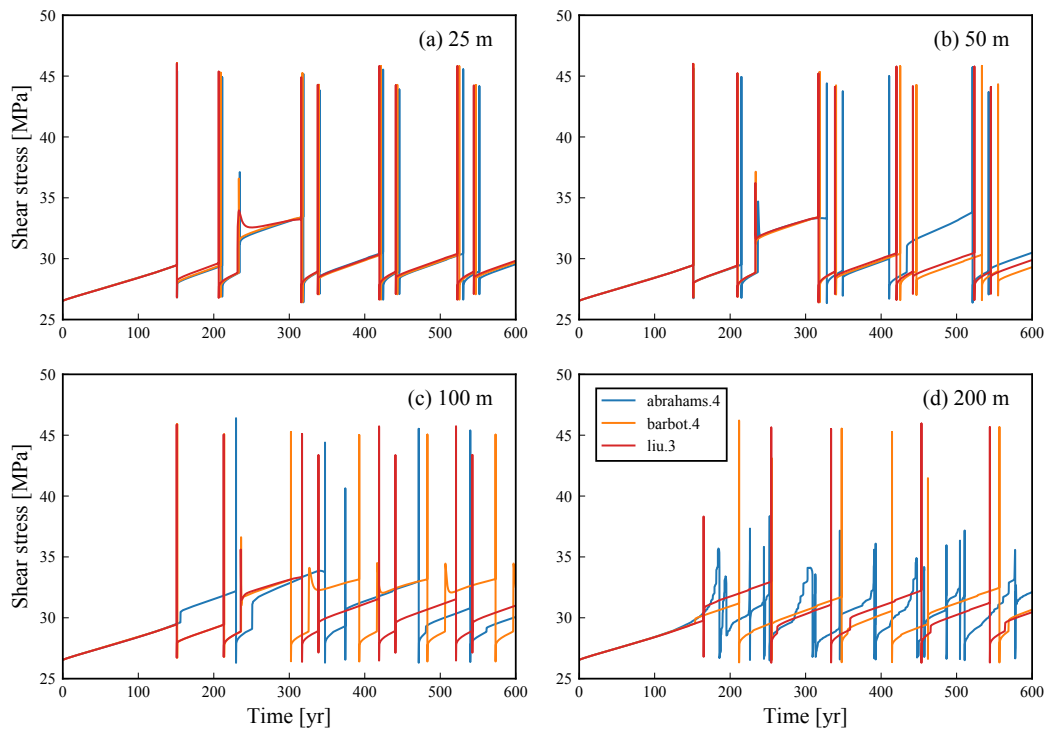


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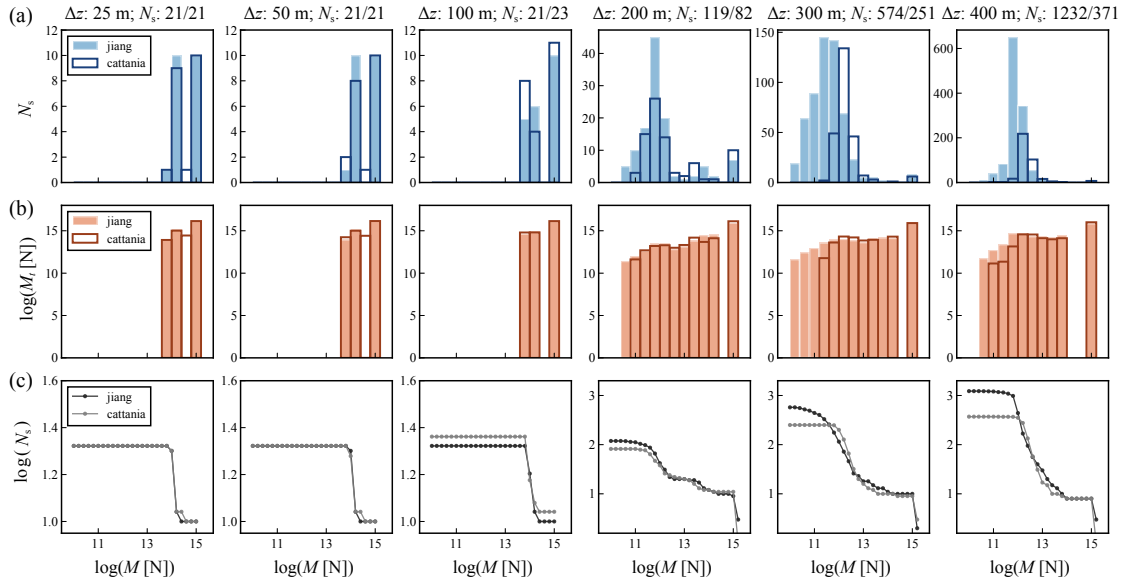


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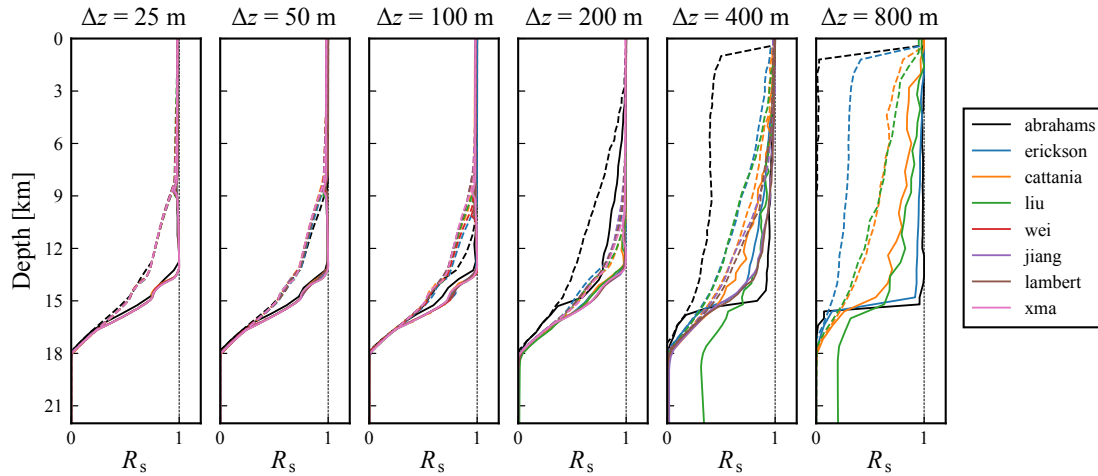


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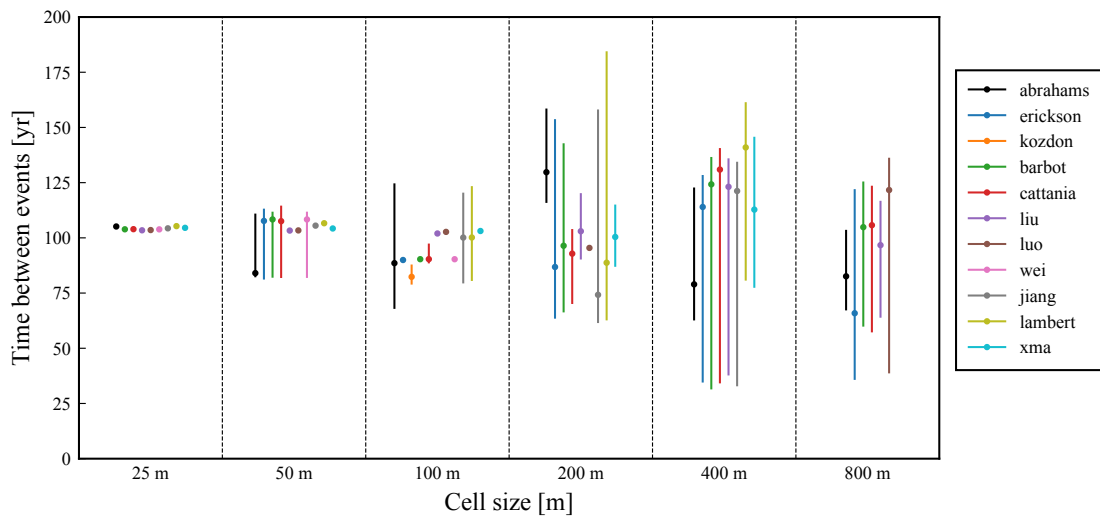


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